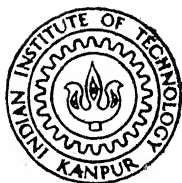


ANALYSIS OF MULTIPHASE SYSTEMS

By
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DEPARTMENT OF ELECTRICAL ENGINEERING
INDIAN INSTITUTE OF TECHNOLOGY, KANPUR

1 MARCH, 1979

ANALYSIS OF MULTIPHASE SYSTEMS

**A Thesis Submitted
In Partial Fulfilment of the Requirements
for the Degree of
MASTER OF TECHNOLOGY**

**By
*AVANISH CHANDRA CHAUBEY***

**to the
DEPARTMENT OF ELECTRICAL ENGINEERING
INDIAN INSTITUTE OF TECHNOLOGY, KANPUR
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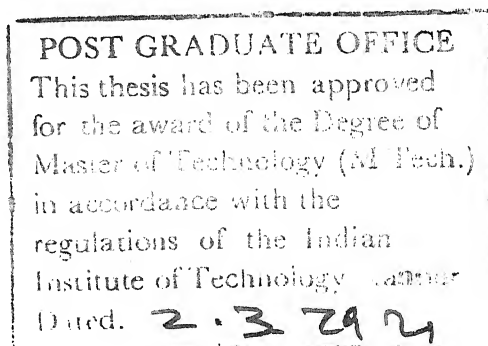


ii

CERTIFICATE

Certified that this work titled "Analysis of Multiphase Systems" by Mr. Avanish Chandra Chaubey has been carried out under my supervision and has not been submitted elsewhere for a degree.

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CONTENTS

	Page
CHAPTER 1 INTRODUCTION	1
CHAPTER 2 SYMMETRIES IN MULTIPHASE NETWORKS	4
2.1 Introduction	4
2.2 Multiphase Power System Networks with Rotational Symmetries	6
(a) 8-phase symmetric element	6
(b) 12-phase system element	14
2.3 Multiphase Power System Networks with Rotational and Reflection Symmetries	25
(a) 8-phase network	25
(b) 12-phase network	29
CHAPTER 3 EIGHT PHASE POWER SYSTEM NETWORK	40
3.1 8-Phase Rotating Element	40
3.2 8-Phase Stationary Element	58
CHAPTER 4 12-PHASE POWER SYSTEM NETWORK	71
4.1 12-Phase Rotating Element	71
4.2 12-Phase Stationary Element	82
CHAPTER 5 CONCLUSION	94
REFERENCES	96
APPENDIX 1 GROUP THEORY	98
APPENDIX 2 ORTHOGONALITY THEOREM	101

ABSTRACT

A multiphase power system network can be subdivided into two classes, one consisting of those elements which possess only rotational symmetries and another of elements which possess both rotational as well as reflection symmetries. The rotational symmetries of an n -phase network consisting of n -fold proper rotations together constitute the cyclic group C_n . The balanced n -phase stationary networks possess reflection symmetries in addition to rotational ones. These symmetries constitute a group C_{nv} consisting of n -fold rotations and n -fold reflections about its axes of symmetries. The group theoretic techniques of dealing with these symmetries have already been used to develop general transformation matrices for 3, 4 and 6-phase systems. This thesis is concerned with developing transformation matrices with complex elements, similar to symmetrical component transformation and with real elements, similar to Clarke's component transformation, for 8 and 12-phase system for the purpose of simplifying the analysis of 8 and 12-phase power system networks. In addition, expressions for sequence impedances and complex power for both 8-phase and 12-phase system, which are useful for the purpose of planning studies and fault analysis are also presented.

CHAPTER 1

INTRODUCTION

Multiphase power systems are currently of major interest on account of the fact that while the demands for electrical energy are steadily on the increase, to find new corridors on land for power system expansion is getting more and more difficult. It is essential, therefore, to try as far as possible, to meet the growing demands by appropriately augmenting the systems on the corridors already in existence. It is in this context multiphase systems have attracted recent attention [2,3]. To design adequate protection system for a power system we have to perform short circuit studies and for this we need to develop suitable methods and transformations for the analysis of such system. Suitable transformations for 4-phase and 6-phase system have been developed recently [1,4,5]. Other higher phase system which will be feasible in future are 8-phase and 12-phase. Our concern here is to extend the group theoretic techniques of analysis to 8-phase and 12-phase systems. Here we have developed the transformations for the purpose of steady state analysis of 8-phase and 12-phase systems. However, following the same procedure transformations for transient analysis can be derived.

The symmetries inherent in multiphase power system networks are:

- (i) Rotational symmetries in space which correspond to physical rotations of networks, known as proper rotations.
- (ii) Rotational symmetries in space followed by reflection about axis of symmetry, known as improper rotations.

Most of the components of a power system network possess rotational symmetries. However, some of the components viz. transmission and distribution networks possess reflection symmetries in addition to rotational ones.

The significant feature of these symmetries is that they satisfy group axioms so that the networks are amenable to the group theoretic techniques. The main advantage of using group theoretic techniques is that by the application of these techniques system equations of a general power system network for the purpose of steady state and transient analysis can be put into a diagonal or at least block diagonal form so that original network can be replaced by a set of smaller disjoint networks whose analysis is straight forward [1,4,5]. Now we give chapterwise description of the thesis.

In Chapter 2, it has been demonstrated that two symmetries viz. rotational symmetry and rotational symmetry followed by reflection symmetry constitute groups and hence can be represented by permutation matrices. These permutation matrices also satisfy group axioms.

Chapter 3 deals with development of suitable transformations for 8-phase power system network analysis using group theoretic

techniques. The symmetries of 8-phase power system network with rotational elements constitute a cyclic group C_8 consisting of 8-fold rotations. The transformation matrix for such network is similar to symmetrical components. The symmetries of 8-phase power system network with stationary elements constitute a group C_{8v} , consisting of 8-fold rotations and 8-fold reflections about the axes of symmetries of the network. The transformation matrix in this case has real elements and is similar to Clarke's component transformation known for 3-phase system. Sequence impedances and expression for complex power are also given.

Chapter 4 deals with development of suitable transformations for 12-phase power system network analysis applying group theoretic techniques. In this chapter, we have presented the two transformation matrices, one with complex basis and other with real basis and expressions for complex power and sequence impedances for 12-phase power system.

CHAPTER 2

SYMMETRIES IN MULTIPHASE NETWORKS

2.1 INTRODUCTION

A power system network used for generation, transmission and distribution of electric power is inherently symmetrical and balanced. These balanced multiphase power system networks can be categorised into two classes, one which consists of only those elements which possess rotational symmetries and other which consist of elements possessing both rotational as well as reflection symmetries. The elements possessing only rotational symmetries are normally referred to as rotational elements whereas the elements possessing both rotational as well as reflection symmetries, stationary elements.

A network is said to be symmetric under a symmetry operation if the system after such an operation is physically indistinguishable from the system before the symmetry operation. With every symmetry operation we can associate a symmetry property which can be attributed to the system which is symmetric under the symmetry operation in question. The two symmetries which are inherently present in the power system networks are reflection symmetry and rotational symmetry.

The reflection symmetry, also referred to as bilateral symmetry is attributed to the symmetry operation of reflection R about the symmetry axis \hat{S} which is equivalent to rotation

through 180° in space about the axis of symmetry of the system. It is obvious that the symmetry operation of reflection if applied twice, brings back the system to the original. This implies that the symmetry operation R is its own inverse. If E be the identity symmetry operation then inverse symmetry operation R^{-1} of symmetry operation of reflection R is same as R , i.e. $R.R = E$ and $R = R^{-1}$.

The rotational symmetry is attributed to the systems which are symmetric under the symmetry operation of rotation C about the axis of rotation passing through centroid O and perpendicular to the plane of the system. The admissible rotation operations will be all those rotations which bring the system into coincidence with the original system. For example, for a n -phase power system possessing rotational symmetry, rotations through $\frac{2\pi}{n}$ degrees (for $m = 1, 2, \dots, n$) are the only admissible rotations. Such rotations are referred to as proper rotation. The general symbol for a proper axis of rotation is C_n where the subscript n denotes the order of the axis. By order is meant the largest value of n such that rotation through $\frac{2\pi}{n}$ gives an equivalent configuration. A rotation by $\frac{2\pi}{n}$ degrees about proper axis C_n is also represented by the symbol C_n . Rotation by $\frac{2\pi}{n}$ degrees carried out m times successively is represented by the symbol C_n^m . It is obvious that rotation C_n^n is rotation by $n \frac{2\pi}{n} = 2\pi$ degrees and hence equal to zero rotation or identity operation E , i.e. $C_n^n = E$. It can be further verified that $C_n^{n+1} = C_n^1 = C_n$ and $C_n^{n+2} = C_n^2 \dots$ etc.

Therefore, it can be observed that a proper axis of order n generates n symmetry operations viz. $C_n^1, C_n^2, \dots, C_n^n (=E)$.

2.2 MULTIPHASE POWER SYSTEM NETWORKS WITH ROTATIONAL SYMMETRY

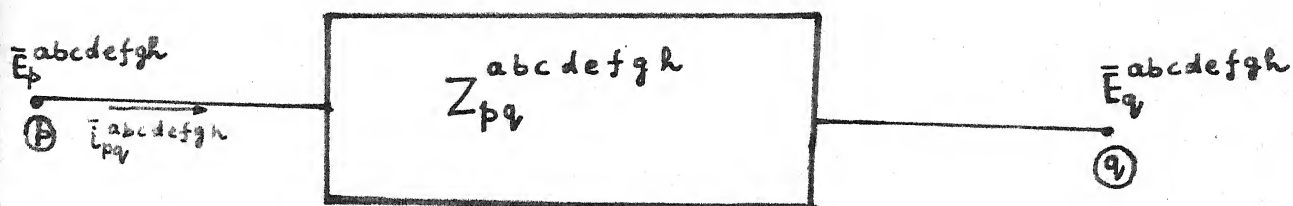
a) 8-Phase Symmetric Element:

Let us consider a 8-phase symmetric (i.e. balanced) power system subnetwork between buses p and q as shown in Figure 2.1. The steady state network equation in the impedance form of this subnetwork will be,

$$\begin{aligned} \bar{E}_p^{abcdefgh} - [Z_{pq}]^{abcdefgh} \bar{i}_{pq}^{abcdefgh} &= \bar{E}_q^{abcdefgh} \\ \text{i.e. } \bar{E}_p^{abcdefgh} - \bar{E}_q^{abcdefgh} &= [Z_{pq}]^{abcdefgh} \bar{i}_{pq}^{abcdefgh} \\ &= \bar{V}_{pq}^{abcdefgh} \quad (2.1) \end{aligned}$$

where $\bar{V}_{pq}^{abcdefgh}$ is the column vector of voltage drops across the 8-phase element $p-q$, $\bar{E}_p^{abcdefgh}$ and $\bar{E}_q^{abcdefgh}$ are the column vectors of bus voltages for the buses p and q respectively and $[Z_{pq}]^{abcdefgh}$ is a 8×8 impedance matrix of a 8-phase element $p-q$. The equation (2.1) can be expressed as

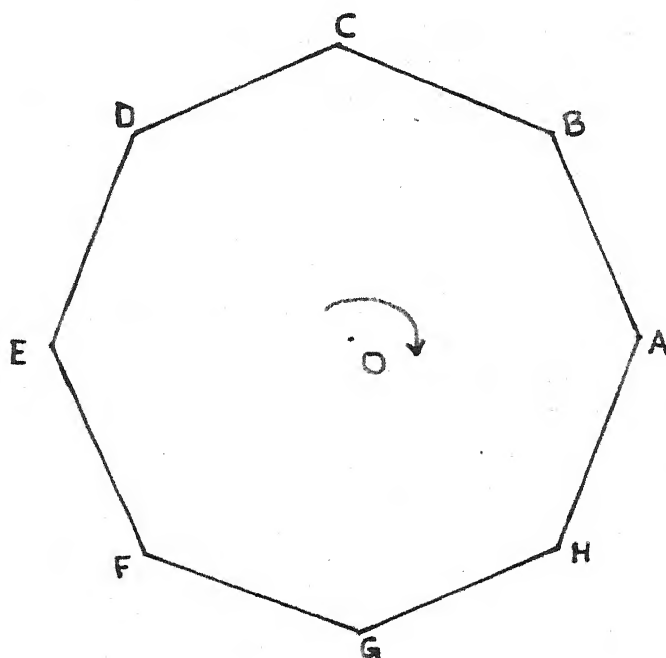
$$\begin{bmatrix} \bar{v}_{pq}^a \\ \bar{v}_{pq}^b \\ \bar{v}_{pq}^c \\ \bar{v}_{pq}^d \\ \bar{v}_{pq}^e \\ \bar{v}_{pq}^f \\ \bar{v}_{pq}^g \\ \bar{v}_{pq}^h \end{bmatrix} = \begin{bmatrix} z_{pq}^{aa} & z_{pq}^{ab} & z_{pq}^{ac} & z_{pq}^{ad} & z_{pq}^{ae} & z_{pq}^{af} & z_{pq}^{ag} & z_{pq}^{ah} \\ z_{pq}^{ba} & z_{pq}^{bb} & z_{pq}^{bc} & z_{pq}^{bd} & z_{pq}^{be} & z_{pq}^{bf} & z_{pq}^{bg} & z_{pq}^{bh} \\ z_{pq}^{ca} & z_{pq}^{cb} & z_{pq}^{cc} & z_{pq}^{cd} & z_{pq}^{ce} & z_{pq}^{cf} & z_{pq}^{cg} & z_{pq}^{ch} \\ z_{pq}^{da} & z_{pq}^{db} & z_{pq}^{dc} & z_{pq}^{dd} & z_{pq}^{de} & z_{pq}^{df} & z_{pq}^{dg} & z_{pq}^{dh} \\ z_{pq}^{ea} & z_{pq}^{eb} & z_{pq}^{ec} & z_{pq}^{ed} & z_{pq}^{ee} & z_{pq}^{ef} & z_{pq}^{eg} & z_{pq}^{eh} \\ z_{pq}^{fa} & z_{pq}^{fb} & z_{pq}^{fc} & z_{pq}^{fd} & z_{pq}^{fe} & z_{pq}^{ff} & z_{pq}^{fg} & z_{pq}^{fh} \\ z_{pq}^{ga} & z_{pq}^{gb} & z_{pq}^{gc} & z_{pq}^{gd} & z_{pq}^{ge} & z_{pq}^{gf} & z_{pq}^{gg} & z_{pq}^{gh} \\ z_{pq}^{ha} & z_{pq}^{hb} & z_{pq}^{hc} & z_{pq}^{hd} & z_{pq}^{he} & z_{pq}^{hf} & z_{pq}^{hg} & z_{pq}^{hh} \end{bmatrix} \begin{bmatrix} \bar{i}_{pq}^a \\ \bar{i}_{pq}^b \\ \bar{i}_{pq}^c \\ \bar{i}_{pq}^d \\ \bar{i}_{pq}^e \\ \bar{i}_{pq}^f \\ \bar{i}_{pq}^g \\ \bar{i}_{pq}^h \end{bmatrix} \quad (2.2)$$



$$\bar{V}_{pq}^{abcdefgh} = \bar{E}_p^{abcdefgh} - \bar{E}_q^{abcdefgh}$$

8-Phase element p-q

FIGURE 2.1



Symmetry Group C_8

FIGURE 2.2

For rotating elements, the symmetries are such that the circularly permuting the port voltages will cause similar permutation of the port currents. These symmetries may equivalently be represented by the physical rotation of the network element as shown diagram-

met. in Figure 2.2 in which vertices ABCDEFGH represent the eight phases. The element shown in this figure is regular octagon with O as centroid. The axis of rotation " δ " passes through O and is perpendicular to the plane of the paper. Considering all possible rotations of octagon about axis δ . We can see only eight rotations out of all possible rotations through different angles (less than or equal to 360°) send the edges and vertices of octagon into coincidence. Therefore, the admissible rotations are rotations through 45° , 90° , 135° , 180° , 225° , 270° , 315° and $360^\circ (= 0)$ about axis δ passing through centroid O and perpendicular to the plane of the paper.

The rotation through 360° which sends the vertices back to their original position is also referred as zero rotation. The permutation table for the zero rotation is given below:

Rotation through 360°	A	B	C	D	E	F	G	H
	A	B	C	D	E	F	G	H

The first clockwise rotation through 45° about axis δ sends the vertex A to H, B to A, C to B, D to C, E to D, F to E, G to F and H to G. This rotation through 45° can be represented by following permutation table:

Rotation through 45°

A	B	C	D	E	F	G	H
H	A	B	C	D	E	F	G

Similarly, other rotations can be represented by the permutation tables given below:

Rotation through 90°

A	B	C	D	E	F	G	H
G	H	A	B	C	D	E	F

Rotation through 135°

A	B	C	D	E	F	G	H
F	G	H	A	B	C	D	E

Rotation through 180°

A	B	C	D	E	F	G	H
E	F	G	H	A	B	C	D

Rotation through 225°

A	B	C	D	E	F	G	H
D	E	F	G	H	A	B	C

Rotation through 270°

A	B	C	D	E	F	G	H
C	D	E	F	G	H	A	B

and

Rotation through 315°

A	B	C	D	E	F	G	H
B	C	D	E	F	G	H	A

If we use the general symbol for proper axis of rotation and rotations, then C_8 is the proper axis of rotation and symmetry operations; $C_8^1, C_8^2, C_8^3, C_8^4, C_8^5, C_8^6, C_8^7$ and $C_8^8 (= E)$ represent the rotations through $45^\circ, 90^\circ, 135^\circ, 180^\circ, 225^\circ, 270^\circ, 315^\circ$ and 360° respectively.

We know that the product of two rotations is same as application of the two rotations successively. It can be seen that application of symmetry operation C_8^1 (rotation through 45°) twice is same as C_8^2 (rotation through 90°), i.e.

$$C_8^1 \cdot C_8^1 = C_8^2$$

The multiplication of all these symmetry operation can be compactly expressed in the form of a group multiplication table, known as Cayley table as shown in Table 1. In this table the entry (a_{ij}) in the i th row and j th column is the product of $a_i \cdot a_j$.

Table 1

	E	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7
E	E	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7
C_8^1	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7	E
C_8^2	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7	E	C_8^1
C_8^3	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7	E	C_8^1	C_8^2
C_8^4	C_8^4	C_8^5	C_8^6	C_8^7	E	C_8^1	C_8^2	C_8^3
C_8^5	C_8^5	C_8^6	C_8^7	E	C_8^1	C_8^2	C_8^3	C_8^4
C_8^6	C_8^6	C_8^7	E	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5
C_8^7	C_8^7	E	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6

Looking at table 1, it is easily verified that symmetry operations $E, C_8^1, C_8^2, C_8^3, C_8^4, C_8^5, C_8^6$ and C_8^7 satisfy the group axioms (Appendix 1) and commutative law. The element E serves as an identity element and C_8^1 is the generator element. Hence, we conclude that the symmetry operations E, C_8^1, C_8^2, \dots and C_8^7 constitute a cyclic group C_8 of order 8. As all the symmetry operations belong to a separate class, the number of classes in the group is also 8.

Now we know that finite groups can be represented by set of matrices $D(R)$ (Appendix 1) such that for every member R of G there is a matrix $D(R)$ in it and there exists a correspondence between the matrices and the group elements such that for any R_1 and R_2 in G ,

$$D(R_1 \cdot R_2) = D(R_1) \cdot D(R_2).$$

The representation matrices $D(R)$ for $R = E, C_8^1, C_8^2, C_8^3, C_8^4, C_8^5, C_8^6$ and C_8^7 are as shown below:

$$D(E) = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} ; \quad D(C_8^1) = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \end{bmatrix}$$

The permutation matrix A has the following properties:

1. $A^T = A^{-1}$
2. $\det A = 1$

In other words, a permutation matrix is orthogonal. Now,

$$\begin{aligned}
 D(\mathcal{C}_8^1)D(\mathcal{C}_8^1) &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \end{bmatrix} \\
 &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix} = D(\mathcal{C}_8^2)
 \end{aligned}$$

Similarly, we can show that

$$D(\mathcal{C}_8^1)D(\mathcal{C}_8^2) = D(\mathcal{C}_8^1)D(\mathcal{C}_8^1)D(\mathcal{C}_8^1) = D(\mathcal{C}_8^3)$$

$$D(\mathcal{C}_8^1)D(\mathcal{C}_8^3) = D(\mathcal{C}_8^1)D(\mathcal{C}_8^1)D(\mathcal{C}_8^1)D(\mathcal{C}_8^1) = D(\mathcal{C}_8^4)$$

$$D(\mathcal{C}_8^1)D(\mathcal{C}_8^4) = D(\mathcal{C}_8^5)$$

$$D(C_8^1)D(C_8^5) = D(C_8^6)$$

$$D(C_8^1)D(C_8^6) = D(C_8^7)$$

$$D(C_8^1)D(C_8^7) = D(C_8^8 = E)$$

It can be verified that

$$D(C_8^2)D(C_8^1) = D(C_8^1)D(C_8^2) = D(C_8^3)$$

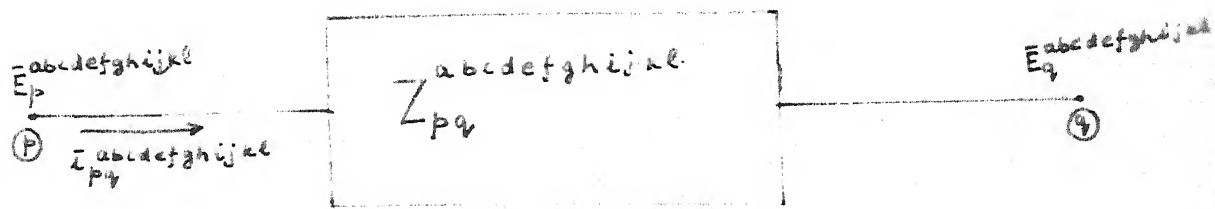
Similarly finding other multiplications of permutation matrices, we can see that the permutation matrices $D(R)$ themselves constitute a cyclic group under multiplication having same multiplication table as for group elements of C_8 . The element $D(C_8^1)$ is the generator element.

b) 12-Phase Symmetry Element:

Now let us consider a 12-phase symmetric power system subnetwork between buses p and q as shown in Figure 2.3. The steady state network equation in the impedance form of this subnetwork is,

$$\begin{aligned} \bar{E}_p^{abcde fghijkl} - \bar{E}_q^{abcde fghijkl} &= [Z_{pq}]^{abcde fghijkl} \bar{I}_{pq}^{abcde fghijkl} \\ &= \bar{V}_{pq}^{abcde fghijkl} \end{aligned} \quad (2.4)$$

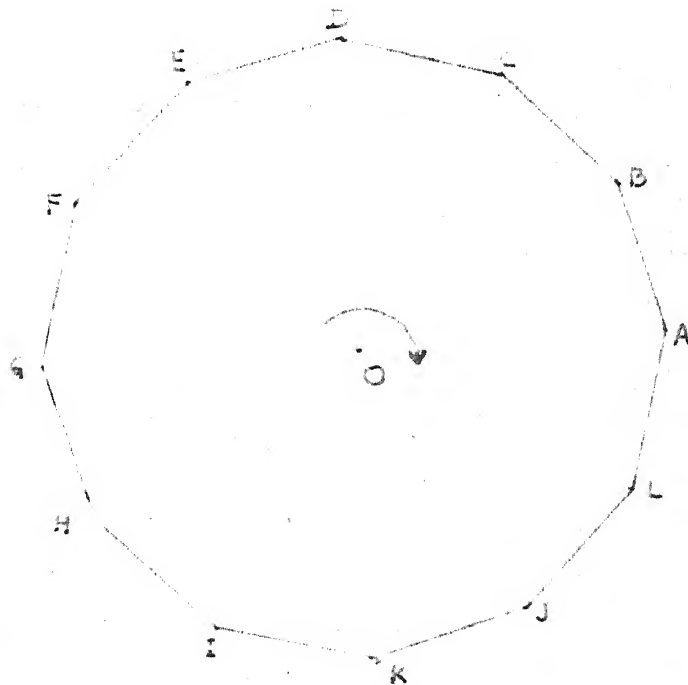
For rotating elements, the symmetries of this network may equivalently be represented by the physical rotation of the regular 12-gon as shown in Figure 2.4. The vertices ABCDEFGHIJKL signify the 12 phases of the network. The axis of rotation δ passes through the centroid O and is perpendicular



$$\bar{V}_{pq}^{\text{a-l}} = \bar{E}_p^{\text{a-l}} - \bar{E}_q^{\text{a-l}}$$

12-Phase element $p-q$

FIGURE 2.3



Symmetry Group C_{12}

FIGURE 2.4

to the plane of the paper. After considering all possible rotations through different angles we find that the admissible rotations about axis δ are rotations through 30° , 60° , 90° , 120° , 150° , 180° , 210° , 240° , 270° , 300° , 330° and 360° . The permutation table for these admissible (clockwise rotations) are given below.

Rotation through 360°
or zero rotation

A B C D E F G H I J K L
A B C D E F G H I J K L

Rotation through 30°

A B C D E F G H I J K L
L A B C D E F G H I J K

Rotation through 60°

A B C D E F G H I J K L
K L A B C D E F G H I J

Rotation through 90°

A B C D E F G H I J K L
J K L A B C D E F G H I

Rotation through 120°

A B C D E F G H I J K L
I J K L A B C D E F G H

Rotation through 150°

A B C D E F G H I J K L
H I J K L A B C D E F G

Rotation through 180°

A B C D E F G H I J K L
G H I J K L A B C D E F

Rotation through 210°

A B C D E F G H I J K L
F G H I J K L A B C D E

Rotation through 240°

A B C D E F G H I J K L
E F G H I J K L A B C D

Rotation through 270°

A B C D E F G H I J K L
D E F G H I J K L A B C

Rotation through 300°

A B C D E F G H I J K L
C D E F G H I J K L A B

Rotation through 330°

A B C D E F G H I J K L
B C D E F G H I J K L A

We can see that the axis of rotation is 12-fold axis and is designated by C_{12} . The rotations through 30° , 60° , 90° , 120° , 150° , 180° , 210° , 240° , 270° , 300° , 330° and 360° are represented by symmetry operations C_{12}^1 , C_{12}^2 , C_{12}^3 , C_{12}^4 , C_{12}^5 , C_{12}^6 , C_{12}^7 , C_{12}^8 , C_{12}^9 , C_{12}^{10} , C_{12}^{11} and $C_{12}^{12} = E$ respectively. The multiplications of all these symmetry operations (rotations) can be expressed by Cayley table given in Table 2.

	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}
E	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}
C_{12}^1	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E
C_{12}^2	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1
C_{12}^3	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2
C_{12}^4	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3
C_{12}^5	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4
C_{12}^6	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5
C_{12}^7	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6
C_{12}^8	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7
C_{12}^9	C_{12}^9	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8
C_{12}^{10}	C_{12}^{10}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9
C_{12}^{11}	C_{12}^{11}	E	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}

Table 2

Looking at table 2, it can be verified that these symmetry operations commute and satisfy the group axioms. The element E is identity element and element C_{12}^1 is the generator element. Hence, the symmetry operations $C_{12}^1, C_{12}^2, \dots, C_{12}^{11}, E$ constitute a cyclic group C_{12} of order 12. The number of classes is 12 as all the group elements in the cyclic group

$$D(C_{12}^{10}) =$$

$$\begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$D(C_{12}^{11}) =$$

$$\begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

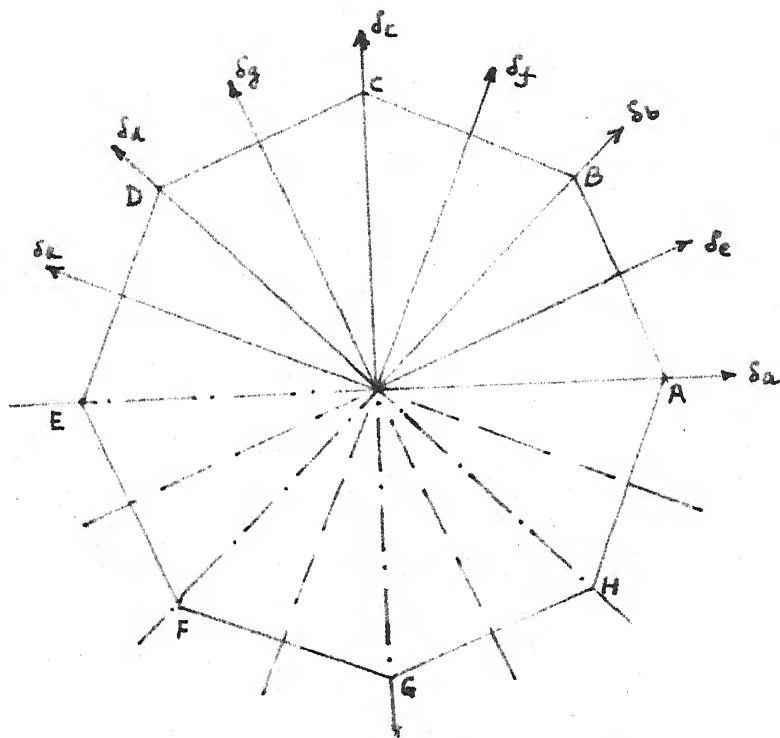
(2.5)

These representation matrices $D(R)$ themselves constitute a cyclic group of order 12 and have $D(C_{12}^1)$ as generator element of the group.

2.3 MULTIPHASE POWER SYSTEM NETWORKS WITH ROTATIONAL AND REFLECTION SYMMETRY

a) 8-Phase network:

We now consider 8-phase symmetric power system networks which possesses in addition to rotational, reflection symmetries also. Symmetries of such network which are normally referred to as stationary element, can be equivalently represented by physical rotation of the network shown in Figure 2.5, about the axis passing through the centroid and perpendicular to the plane of the paper and also reflections of the network about the axes of symmetries. The network configuration remains invariant under rotations by 45° , 90° , 135° , 180° , 225° , 270° , 315° and 360° and also under reflection about axes of symmetry. The axes of symmetries in this case of the network in Figure 2.5, which is a regular octagon are lines joining opposite vertices and lines joining mid-points of opposite edges. These axes of symmetries are denoted by δ_a , δ_b , δ_c , δ_d , δ_e , δ_f , δ_g , and δ_h in the figure. For networks with stationary elements, in all we have sixteen symmetry operations viz. C_8^1 , C_8^2 , C_8^3 , C_8^4 , C_8^5 , C_8^6 , C_8^7 , and E representing rotations through 45° , 90° , 135° , 180° , 225° , 270° , 315° and 360° respectively and δ'_a , δ'_b , δ'_c , δ'_d , δ'_e , δ'_f , δ'_g and δ'_h representing reflections about axes of symmetries δ_a , δ_b , δ_c , δ_d , δ_e , δ_f , δ_g , and δ_h respectively. The Cayley's multiplication table for these sixteen symmetry operations is given in Table 3.



Symmetric Group C_{8v}

FIGURE 2-5

TABLE 3

	\mathbb{E}	c_8^1	c_8^2	c_8^3	c_8^4	c_8^5	c_8^6	c_8^7	δ_a^1	δ_b^1	δ_c^1	δ_d^1	δ_e^1	δ_f^1	δ_g^1	δ_h^1
\mathbb{E}	\mathbb{E}	c_8^1	c_8^2	c_8^3	c_8^4	c_8^5	c_8^6	c_8^7	δ_a^1	δ_b^1	δ_c^1	δ_d^1	δ_e^1	δ_f^1	δ_g^1	δ_h^1
c_8^1	c_8^1	c_8^2	c_8^3	c_8^4	c_8^5	c_8^6	c_8^7	\mathbb{E}	δ_e^1	δ_f^1	δ_g^1	δ_h^1	δ_b^1	δ_c^1	δ_d^1	δ_a^1
c_8^2	c_8^2	c_8^3	c_8^4	c_8^5	c_8^6	c_8^7	\mathbb{E}	c_8^1	δ_b^1	δ_c^1	δ_d^1	δ_a^1	δ_f^1	δ_g^1	δ_h^1	δ_e^1
c_8^3	c_8^3	c_8^4	c_8^5	c_8^6	c_8^7	\mathbb{E}	c_8^1	c_8^2	δ_f^1	δ_g^1	δ_h^1	δ_e^1	δ_c^1	δ_d^1	δ_a^1	δ_b^1
c_8^4	c_8^4	c_8^5	c_8^6	c_8^7	\mathbb{E}	c_8^1	c_8^2	c_8^3	δ_c^1	δ_d^1	δ_a^1	δ_b^1	δ_g^1	δ_h^1	δ_e^1	δ_f^1
c_8^5	c_8^5	c_8^6	c_8^7	\mathbb{E}	c_8^1	c_8^2	c_8^3	c_8^4	δ_g^1	δ_h^1	δ_e^1	δ_f^1	δ_d^1	δ_a^1	δ_b^1	δ_c^1
c_8^6	c_8^6	c_8^7	\mathbb{E}	c_8^1	c_8^2	c_8^3	c_8^4	c_8^5	δ_d^1	δ_a^1	δ_b^1	δ_c^1	δ_h^1	δ_e^1	δ_f^1	δ_g^1
c_8^7	c_8^7	\mathbb{E}	c_8^1	c_8^2	c_8^3	c_8^4	c_8^5	c_8^6	δ_h^1	δ_e^1	δ_f^1	δ_g^1	δ_a^1	δ_b^1	δ_c^1	δ_d^1
δ_a^1	δ_a^1	δ_e^1	δ_b^1	δ_f^1	δ_c^1	δ_g^1	δ_d^1	δ_h^1	\mathbb{E}	c_8^2	c_8^4	c_8^6	c_8^1	c_8^3	c_8^5	c_8^7
δ_b^1	δ_b^1	δ_f^1	δ_c^1	δ_g^1	δ_d^1	δ_h^1	δ_a^1	δ_e^1	c_8^6	\mathbb{E}	c_8^2	c_8^4	c_8^7	c_8^1	c_8^3	c_8^5
δ_c^1	δ_c^1	δ_g^1	δ_d^1	δ_h^1	δ_a^1	δ_e^1	δ_b^1	δ_f^1	c_8^4	c_8^6	\mathbb{E}	c_8^2	c_8^5	c_8^7	c_8^1	c_8^3
δ_d^1	δ_d^1	δ_h^1	δ_a^1	δ_e^1	δ_b^1	δ_f^1	δ_c^1	δ_g^1	c_8^2	c_8^4	c_8^6	\mathbb{E}	c_8^3	c_8^5	c_8^7	c_8^1
δ_e^1	δ_e^1	δ_b^1	δ_f^1	δ_c^1	δ_g^1	δ_d^1	δ_h^1	δ_a^1	c_8^7	c_8^1	c_8^3	c_8^5	\mathbb{E}	c_8^2	c_8^4	c_8^6
δ_f^1	δ_f^1	δ_c^1	δ_g^1	δ_d^1	δ_h^1	δ_a^1	δ_e^1	δ_b^1	c_8^5	c_8^7	c_8^1	c_8^3	c_8^6	\mathbb{E}	c_8^2	c_8^4
δ_g^1	δ_g^1	δ_d^1	δ_h^1	δ_a^1	δ_e^1	δ_b^1	δ_f^1	δ_c^1	c_8^3	c_8^5	c_8^7	c_8^1	c_8^4	c_8^6	\mathbb{E}	c_8^2
δ_h^1	δ_h^1	δ_a^1	δ_e^1	δ_b^1	δ_f^1	δ_c^1	δ_g^1	δ_d^1	c_8^1	c_8^3	c_8^5	c_8^7	c_8^2	c_8^4	c_8^6	\mathbb{E}

Looking at Table 3, we verify that these symmetry operations constitute a symmetry group O_{8v} . The group elements are eight rotation operations and eight reflection operations about symmetry axes. The identity element of the group is E.

These symmetry operations which constitute the group O_{8v} , can be represented by permutation matrices. The permutation matrices representing symmetry operation of rotations are same as given in Eqn.(2.3). The permutation matrices representing reflections about axes of symmetries viz. $s'_a, s'_b, s'_c, s'_d, s'_e, s'_f, s'_g$ and s'_h are given below.

$$D(s'_a) = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$D(s'_b) = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$D(s'_c) = \begin{bmatrix} 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix}$$

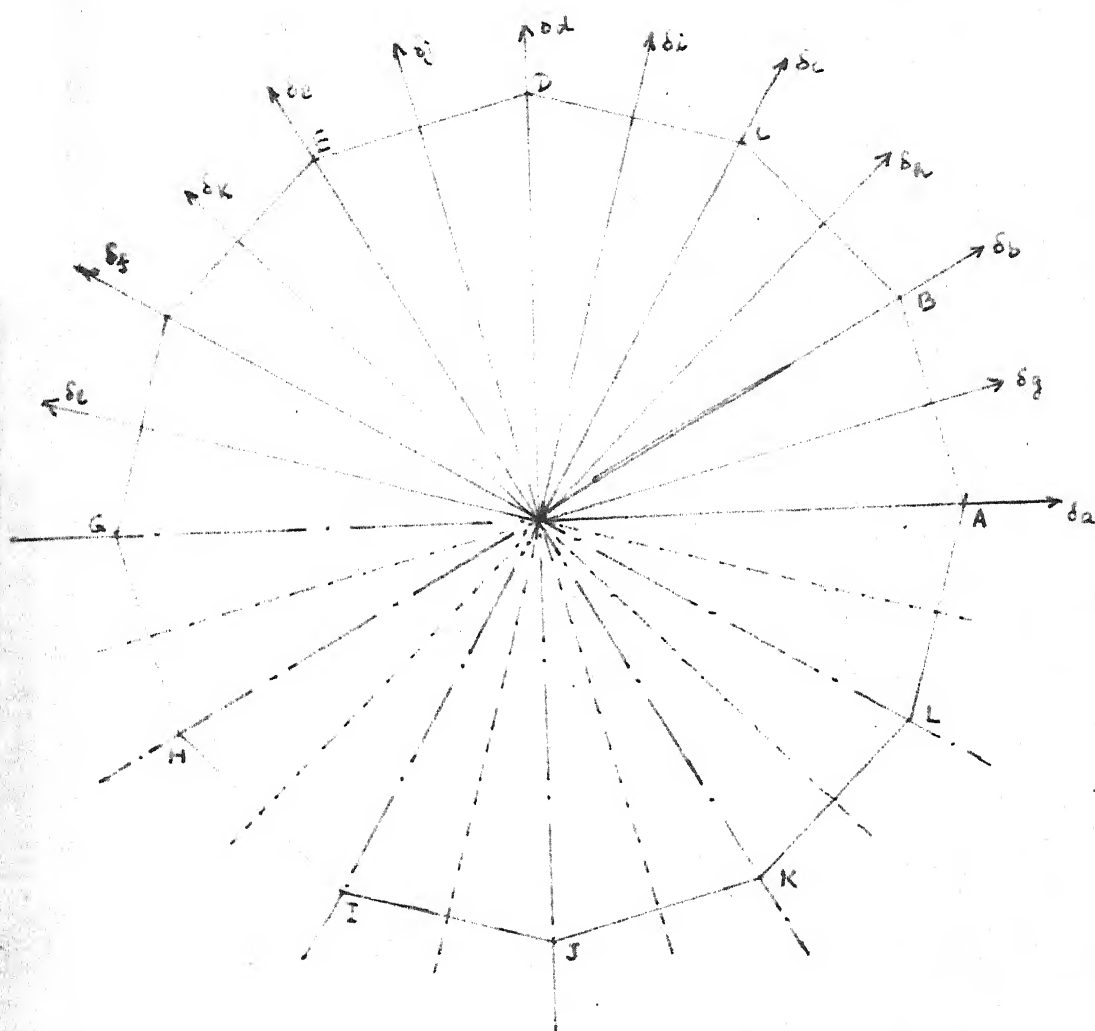
$$D(s'_d) = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{aligned}
 D(\delta'_e) &= \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} & D(\delta'_f) &= \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \end{bmatrix} \\
 D(\delta'_g) &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \end{bmatrix} & D(\delta'_h) &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}
 \end{aligned} \tag{2.6}$$

It can be easily verified that these permutation matrices also constitute a group under multiplication having same multiplication table as that for corresponding elements of group C_{8v} .

b) 12-Phase network:

The symmetries of 12-phase power system network with stationary elements can be represented by physical rotation of the network shown in Figure 2.6 about the axis passing through centroid and perpendicular to the plane of the paper and reflections of the network about the axes of symmetries.



Symmetry Group C_{12v}

FIGURE 2-6

The axis of rotation is 12-fold axis in this case and the rotations are through 30° , 60° , 90° , 120° , 150° , 180° , 210° , 240° , 270° , 300° , 330° and 360° represented by symmetry group elements C_{12}^1 , C_{12}^2 , ..., C_{12}^{11} and $C_{12}^{12} = E$ respectively. The axes of reflection are lines joining opposite vertices viz. δ_a , δ_b , δ_c , δ_d , δ_e , and δ_f and lines joining mid points of the opposite edges viz. δ_g , δ_h , δ_i , δ_j , δ_k , and δ_l . The symmetry operations representing reflections about δ_a , δ_b , δ_c , δ_d , δ_e , δ_f , δ_g , δ_h , δ_i , δ_j , δ_k and δ_l are δ'_a , δ'_b , δ'_c , δ'_d , δ'_e , δ'_f , δ'_g , δ'_h , δ'_i , δ'_j , δ'_k and δ'_l respectively. The Cayley's multiplication table for these symmetry operations is given in Table 4. Looking at the Table 4 we can verify that these twenty four symmetry operations constitute a symmetry group \mathcal{U}_{12v} . The group elements are twelve symmetry operations of rotation and twelve symmetry operations of reflection.

Just like 8-phase symmetric systems, these symmetry operations can be represented by permutation matrices. The permutation matrices representing rotation operations are same as given in Eqn.(2.5). The permutation matrices representing reflection operations are given in Eqn.(2.7).

It can be verified that these permutation matrices also constitute a group under multiplication having the same multiplication table as that for corresponding elements of group \mathcal{U}_{12v} .

$$D(\delta'_c) =$$

0	0	0	0	1	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0

$$D(\delta'_d) =$$

0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0

$$D(\delta'_{gg}) =$$

0	1	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	1	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0

$$\mathbb{D}(\delta_h') =$$

0	0	0	1	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	0	1	0	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0

$$D(\delta_i^1) =$$

0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	0	1	0	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0

$$D(\delta_j^1) =$$

0	0	0	0	0	0	0	1	0	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	0	1	0	0	0

CHAPTER 3

EIGHT PHASE POWER SYSTEM NETWORKS

In the previous chapter we have seen that symmetries of multiphase systems can be represented by permutation matrices $D(R)$. In this chapter, we extend the group theoretic techniques to develop suitable transformations for the purposes of steady state as well as transient analysis of 8-phase power systems.

3.1 8-PHASE ROTATING ELEMENTS

For rotating elements, the symmetries are such that circularly permuting port voltages will cause similar permutations of the port currents, i.e. if the voltage vector $\bar{v}_{pq}^{abcdefgh}$ is changed to $D(R)\bar{v}_{pq}^{abcdefgh}$ then correspondingly the current vector $\bar{i}_{pq}^{abcdefgh}$ is replaced by $D(R)\bar{i}_{pq}^{abcdefgh}$. Hence, from equation (2.1), we get

$$D(R) \bar{v}_{pq}^{abcdefgh} = [Z_{pq}]^{abcdefgh} D(R) \bar{i}_{pq}^{abcdefgh}$$

$$\text{or} \quad \bar{v}_{pq}^{abcdefgh} = D^{-1}(R) [Z_{pq}]^{abcdefgh} D(R) \bar{i}_{pq}^{abcdefgh} \quad (3.1)$$

Comparing equation (2.2) and (3.1), we get

$$[Z_{pq}]^{abcdefgh} = D^{-1}(R) [Z_{pq}]^{abcdefgh} D(R)$$

$$\text{Taking } R = C_8^1, \quad D^{-1}(R) = D^{-1}(C_8^1) = D(C_8^7)$$

$$[Z_{pq}]^{abcdefgh} = D(C_8^7) [Z_{pq}]^{abcdefgh} D(C_8^1) \quad (3.2)$$

Comparing two matrices, we get

$$\begin{aligned}
 z_{pq}^{aa} &= z_{pq}^{bb} = z_{pq}^{cc} = z_{pq}^{dd} = z_{pq}^{ee} = z_{pq}^{ff} = z_{pq}^{gg} = z_{pq}^{hh} = z_{pq}^s \quad (\text{say}) \\
 z_{pq}^{ab} &= z_{pq}^{bc} = z_{pq}^{cd} = z_{pq}^{de} = z_{pq}^{ef} = z_{pq}^{fg} = z_{pq}^{gh} = z_{pq}^{ha} = z_{pq}^{m1} \quad (\text{say}) \\
 z_{pq}^{ac} &= z_{pq}^{ce} = z_{pq}^{eg} = z_{pq}^{ga} = z_{pq}^{hb} = z_{pq}^{bd} = z_{pq}^{df} = z_{pq}^{fh} = z_{pq}^{m2} \quad (\text{say}) \\
 &\vdots \\
 &\vdots \\
 &\vdots \\
 z_{pq}^{ah} &= z_{pq}^{hg} = z_{pq}^{gf} = z_{pq}^{fe} = z_{pq}^{ed} = z_{pq}^{dc} = z_{pq}^{cb} = z_{pq}^{ba} = z_{pq}^{m7} \quad (\text{say}) \quad (3.3)
 \end{aligned}$$

From (3.3) we can see that, impedance matrix z_{pq} is cyclic and of the form:

$$\begin{bmatrix}
 z_{pq}^s & z_{pq}^{m1} & z_{pq}^{m2} & z_{pq}^{m3} & z_{pq}^{m4} & z_{pq}^{m5} & z_{pq}^{m6} & z_{pq}^{m7} \\
 z_{pq}^{m7} & z_{pq}^s & z_{pq}^{m1} & z_{pq}^{m2} & z_{pq}^{m3} & z_{pq}^{m4} & z_{pq}^{m5} & z_{pq}^{m6} \\
 z_{pq}^{m6} & z_{pq}^{m7} & z_{pq}^s & z_{pq}^{m1} & z_{pq}^{m2} & z_{pq}^{m3} & z_{pq}^{m4} & z_{pq}^{m5} \\
 z_{pq}^{m5} & z_{pq}^{m6} & z_{pq}^{m7} & z_{pq}^s & z_{pq}^{m1} & z_{pq}^{m2} & z_{pq}^{m3} & z_{pq}^{m4} \\
 z_{pq}^{m4} & z_{pq}^{m5} & z_{pq}^{m6} & z_{pq}^{m7} & z_{pq}^s & z_{pq}^{m1} & z_{pq}^{m2} & z_{pq}^{m3} \\
 z_{pq}^{m3} & z_{pq}^{m4} & z_{pq}^{m5} & z_{pq}^{m6} & z_{pq}^{m7} & z_{pq}^s & z_{pq}^{m1} & z_{pq}^{m2} \\
 z_{pq}^{m2} & z_{pq}^{m3} & z_{pq}^{m4} & z_{pq}^{m5} & z_{pq}^{m6} & z_{pq}^{m7} & z_{pq}^s & z_{pq}^{m1} \\
 z_{pq}^{m1} & z_{pq}^{m2} & z_{pq}^{m3} & z_{pq}^{m4} & z_{pq}^{m5} & z_{pq}^{m6} & z_{pq}^{m7} & z_{pq}^s
 \end{bmatrix} \quad (3.4)$$

Now, the eigenvectors of permutation matrices (Eqn.2.3) are given by the following matrix A_c [11]:

$$A_c = \frac{1}{\sqrt{8}} \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 \\ 1 & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a \\ 1 & a^3 & a^4 & a^5 & a^6 & a^7 & a & a^2 \\ 1 & a^4 & a^5 & a^6 & a^7 & a & a^2 & a^3 \\ 1 & a^5 & a^6 & a^7 & a & a^2 & a^3 & a^4 \\ 1 & a^6 & a^7 & a & a^2 & a^3 & a^4 & a^5 \\ 1 & a^7 & a & a^2 & a^3 & a^4 & a^5 & a^6 \end{bmatrix}$$

where $a = \underline{8/1} = e^{j2\pi/8} = 1\angle 45^\circ = \frac{1}{\sqrt{2}}(1+j)$

$$a^2 = j, \quad a^3 = \frac{1}{\sqrt{2}}(-1+j) = -a^*, \quad a^4 = -1,$$

$$a^5 = -\frac{1}{\sqrt{2}}(1+j) = -a, \quad a^6 = -j = -a^2$$

and $a^7 = \frac{1}{\sqrt{2}}(1-j) = a^*$

So

$$A_c = \frac{1}{\sqrt{8}} \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a & a^2 & -a^* & -1 & -a & -a^2 & a^* \\ 1 & a^2 & -a^* & -1 & -a & -a^2 & a^* & a \\ 1 & -a^* & -1 & -a & -a^2 & a^* & a & a^2 \\ 1 & -1 & -a & -a^2 & a^* & a & a^2 & -a^* \\ 1 & -a & -a^2 & a^* & a & a^2 & -a^* & -1 \\ 1 & -a^2 & a^* & a & a^2 & -a^* & -1 & -a \\ 1 & a^* & a & a^2 & -a^* & -1 & -a & -a^2 \end{bmatrix} \quad (3.5)$$

The unitary matrix A_c , whose columns are eigenvector of $D(R)$, will diagonalize each of the permutation matrices $D(R)$ for $R = C_8^1, C_8^2, \dots, C_8^7, E$, i.e.

$$A_c^{*T} D(R) A_c = \text{Diag} D(R)$$

The coefficient matrix $[Z_{pq}]$ commutes with the permutation matrices and therefore the same unitary matrix will also diagonalize the coefficient matrix $[Z_{pq}]$. It is evident that the unitary matrix A_c is similar to the symmetrical component transformation matrix for a 3-phase system.

Now we will rederive the transformation for the eight phase cyclic symmetries using representation theory approach [1,5,6,8,14].

Representation Theory Approach:

A representation $D(R)$ is said to be reducible if its matrices can be expressed as direct sums of matrices of smaller dimension obtained by a similarity transformation to each matrix of the group. Otherwise it is said to be irreducible. Let $D(R)$ be a representation of a group S containing elements (R) . Then, for a nonsingular matrix α , let $\bar{D}(R)$ be the similarity transformation of $D(R)$ under α , i.e.

$$\bar{D}(R) = \alpha^{-1} D(R) \alpha$$

Thus a reducible representation can be converted to block diagonal form, called reduced out representation via a similarity transformation. It is generally understood that

transformation matrix α is unitary, i.e. $\alpha^{-1} = \alpha^{*T}$. The submatrix blocks on the diagonal of the reduced out representation are the irreducible representation of the group, i.e.

$$\bar{D}(R) = \alpha^{*T} D(R) \alpha = \begin{bmatrix} D^1(R) & & & 0 \\ & D^2(R) & & \\ & & \ddots & \\ 0 & & & \ddots \end{bmatrix} \quad (3.6)$$

where $D^1(R)$, $D^2(R)$... etc. are irreducible representations of the group not necessarily distinct. For any representation irreducible or not, an important set of invariants is that of its characters which are traces of the matrices of representations, i.e. characters of equivalent representations are the same.

We now give some important rules about irreducible representations and their characters which are the consequences of the orthogonality theorem (Appendix 2).

1. The sum of squares of the dimensions of the irreducible representations is equal to the order of the group, i.e. number of distinct elements of the group i.e.

$$\sum l_i^2 = l_1^2 + l_2^2 + \dots = h \quad (3.7)$$

where h is order of the group and l_i is dimension of i th irreducible representation.

2. The sum of squares of characters in any irreducible representations is equal to the order of the group, i.e.

$$\sum_R (X^i(R))^2 = h \quad (3.8)$$

where $X^i(R)$ is the character of i th irreducible representation.

3. The vectors whose components are the characters of two different irreducible representations are orthogonal, i.e.

$$\sum_R X^i(R) X^j(R)^* = 0 \quad \text{for } i \neq j \quad (3.9)$$

4. In a given representation (reducible or irreducible) characters of all matrices belonging to the symmetry operation in the same class are identical, and

5. The number of irreducible representations in a group is equal to the number of classes in the group.

As already mentioned, any reducible matrix can be reduced to a similar matrix consisting of blocks on the diagonal via a similarity transformation α . Since the character, i.e. trace of matrix is not changed by similarity transformation, we have

$$X(R) = \sum_j a_j X^j(R)$$

where $X(R)$ is character of i th reducible representation, $X^j(R)$ is that of j th irreducible representation, a_j is number of times the irreducible representation $D^j(R)$ appears in the block diagonal of reduced out representation $\bar{D}(R)$ of $D(R)$.

From above we get

$$a_j = \frac{1}{h} \sum X(R) X^j(R) \quad (3.10)$$

and $\bar{D}(R)$ will be of the form

$$\bar{D}(R) = \alpha^{*T} D(R) \alpha$$

$$= \begin{bmatrix} D^1(R) & & & & \\ & D^2(R) & & & \\ & & \ddots & & \\ & & & D^j(R) & \\ & & & & D^j(R) \\ & & & & & \ddots \\ & & & & & & D^j(R) \\ & & & & & & & \ddots \end{bmatrix} \quad (3.11)$$

Now, we consider block diagonalization of matrices which commute with $D(R)$. The similarity transformation α which block diagonalizes $D(R)$ has a significant property [12,13,1] that it also diagonalizes matrices which commute with $D(R)$. Let α be the transformation which reduces $D(R)$ to the block diagonal form given by equation (3.11), in which j th irreducible representation is of dimension l_j and repeats a_j times in the block diagonal. Let A be the matrix which commutes with $D(R)$, i.e.

$$A D(R) = D(R) A$$

Then, α also transforms A into a block diagonal form \bar{A} .

$$\bar{A} = \alpha^{*T} A \alpha =$$

$$\begin{bmatrix} \bar{A}_1 & & & & & & & 0 \\ & \bar{A}_2 & & & & & & \\ & & \ddots & & & & & \\ & & & \bar{A}_j & & & & \\ & & & & \ddots & & & \\ & & & & & \bar{A}_j & & \\ & & & & & & \ddots & \\ 0 & & & & & & & \bar{A}_k \end{bmatrix}$$

where \bar{A}_j repeats l_j times on the diagonal of \bar{A} , and is of dimension a_j corresponding to the irreducible representation $D^j(R)$.

We have shown in Chapter 2 that permutation matrices (Eqn. 2.3) representing rotation 1 symmetries of a 8-phase power system network form a cyclic group of order 8 and each element of group is in a separate class. Therefore, the number of classes in group C_8 will be equal to 8 and the number of irreducible representations which are equal to the number of classes, will also be equal to 8. Let l_1, l_2, \dots, l_8 be the dimensions of these irreducible representations, then from Eqn.(3.7), we get,

$$\sum_{i=1}^8 l_i^2 = l_1^2 + l_2^2 + \dots + l_8^2 = 8$$

$$\text{i.e.} \quad l_1 = l_2 = l_3 = l_4 = l_5 = l_6 = l_7 = l_8 = 1$$

Therefore, all the irreducible representations have the dimension equal to 1. Likewise, from Eqn.(3.8),

$$\sum x_i^2(R) = 8$$

and hence the characters $X^i(R)$ are each of unity modulus. Using standard computational techniques based on the orthogonality theorem (Appendix 2), one then gets the character table shown below:

C_8	E	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7	
$X^1(R)$	1	1	1	1	1	1	1	1	
$X^2(R)$	1	a	a^2	a^3	a^4	a^5	a^6	a^7	
$X^3(R)$	1	a^2	a^3	a^4	a^5	a^6	a^7	a	
$X^4(R)$	1	a^3	a^4	a^5	a^6	a^7	a	a^2	(3.13)
$X^5(R)$	1	a^4	a^5	a^6	a^7	a	a^2	a^3	
$X^6(R)$	1	a^5	a^6	a^7	a	a^2	a^3	a^4	
$X^7(R)$	1	a^6	a^7	a	a^2	a^3	a^4	a^5	
$X^8(R)$	1	a^7	a	a^2	a^3	a^4	a^5	a^6	
Red. Rep. $X(R)$	8	0	0	0	0	0	0	0	

CHARACTER TABLE

where $a = e^{j2\pi/8} = \frac{1}{\sqrt{2}}(1+j)$

Evidently in this case, the character table itself gives the irreducible representation of the group,

\mathbb{C}_8	E	\mathbb{C}_8^1	\mathbb{C}_8^2	\mathbb{C}_8^3	\mathbb{C}_8^4	\mathbb{C}_8^5	\mathbb{C}_8^6	\mathbb{C}_8^7
$D^1(R)$	1	1	1	1	1	1	1	1
$D^2(R)$	1	a	a^2	a^3	a^4	a^5	a^6	a^7
$D^3(R)$	1	a^2	a^3	a^4	a^5	a^6	a^7	a
$D^4(R)$	1	a^3	a^4	a^5	a^6	a^7	a	a^2
$D^5(R)$	1	a^4	a^5	a^6	a^7	a	a^2	a^3
$D^6(R)$	1	a^5	a^6	a^7	a	a^2	a^3	a^4
$D^7(R)$	1	a^6	a^7	a	a^2	a^3	a^4	a^5
$D^8(R)$	1	a^7	a	a^2	a^3	a^4	a^5	a^6

(3.14)

IRREDUCIBLE REPRESENTATION

The number of times each of these irreducible representations, $D^i(R)$ appear at the diagonal of the reduced out representation $\overline{D}(R)$ is from Eqn.(3.10),

$$a_i = \frac{1}{h} \sum_R X^i(R) X(R)$$

$$a_1 = \frac{1}{8} \sum_R X^1(R) X(R) = \frac{1}{8} (1(8) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0)) = 1$$

$$a_2 = \frac{1}{8} \sum_R X^2(R) X(R) = \frac{1}{8} (1(8) + a(0) + a^2(0) + a^3(0) + a^4(0) + a^5(0) + a^6(0) + a^7(0)) = 1$$

Similarly, we get

$$a_3 = a_4 = a_5 = a_6 = a_7 = a_8 = 1$$

Therefore, $\bar{D}(R)$ is of the form:

$$\bar{D}(R) = \begin{bmatrix} D^1(R) & & & & & & & \\ & D^2(R) & & & & & & \\ & & D^3(R) & & & & & \\ & & & D^4(R) & & & & \\ & & & & D^5(R) & & & \\ & & & & & D^6(R) & & \\ & & & & & & D^7(R) & \\ & & & & & & & D^8(R) \\ & & & & & & & & 0 \end{bmatrix} \quad (3.15)$$

In order to determine the similarity transformation α , the following matrix based upon the orthogonality theorem is constructed [12, 13, 14, 16] i.e.

$$G_i^j = \sum_R D^j(R)_{ii} D(R) \quad (3.16)$$

where $D^j(R)_{ii}$ is the diagonal element of the irreducible representation $D^j(R)$ for $j = 1, 2, \dots, 8$ counting i once for every appearance of reducible representation $D(R)$. Then, the basis vector α_{mnp} , where α_{mnp} denotes the p th linear independent vector corresponding to m th irreducible representation appearing for n th time, is constructed by scanning matrices G_i^j from left to right and picking first the linearly independent columns of G_1^1 , then of G_1^2 , G_1^3 , G_1^4 , G_1^5 , G_1^6 , G_1^7 and G_1^8 . Now from Eqn.(3.16) we have

$$G_1^1 = \sum_R D^1(R)_{11} D(R) = D^1(E)_{11} D(E) + D^1(R_1)_{11} D(R_1) + D^1(R_2)_{11} D(R_2) \\ + D^1(R_3)_{11} D(R_3) + D^1(R_4)_{11} D(R_4) + D^1(R_5)_{11} D(R_5) \\ + D^1(R_6)_{11} D(R_6) + D^1(R_7)_{11} D(R_7)$$

where $R_1 = \mathcal{C}_8^1$, $R_2 = \mathcal{C}_8^2$, $R_3 = \mathcal{C}_8^3$, $R_4 = \mathcal{C}_8^4$, $R_5 = \mathcal{C}_8^5$, $R_6 = \mathcal{C}_8^6$,

and $R_7 = \mathcal{C}_8^7$

$$= 1 D(E) + 1 D(R_1) + 1 D(R_2) + 1 D(R_3) + 1 D(R_4) + 1 D(R_5) \\ + 1 D(R_6) + 1 D(R_7)$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix}$$

$$G_1^2 = \sum_R D^2(R)_{11} D(R)$$

$$= 1 D(E) + a D(R_1) + a^2 D(R_2) + a^3 D(R_3) + a^4 D(R_4) + a^5 D(R_5) \\ + a^6 D(R_6) + a^7 D(R_7)$$

$$= \begin{bmatrix} 1 & a^7 & a^6 & a^5 & a^4 & a^3 & a^2 & a \\ a & 1 & a^7 & a^6 & a^5 & a^4 & a^3 & a^2 \\ a^2 & a & 1 & a^7 & a^6 & a^5 & a^4 & a^3 \\ a^3 & a^2 & a & 1 & a^7 & a^6 & a^5 & a^4 \\ a^4 & a^3 & a^2 & a & 1 & a^7 & a^6 & a^5 \\ a^5 & a^4 & a^3 & a^2 & a & 1 & a^7 & a^6 \\ a^6 & a^5 & a^4 & a^3 & a^2 & a & 1 & a^7 \\ a^7 & a^6 & a^5 & a^4 & a^3 & a^2 & a & 1 \end{bmatrix}$$

$$G_1^3 = \sum_R D^3(R)_{11} D(R) = 1 D(E) + a^2 D(R_1) + a^3 D(R_2) + a^4 D(R_3) + a^5 D(R_4) \\ + a^6 D(R_5) + a^7 D(R_6) + a D(R_7)$$

$$= \begin{bmatrix} 1 & a & a^7 & a^6 & a^5 & a^4 & a^3 & a^2 \\ a^2 & 1 & a & a^7 & a^6 & a^5 & a^4 & a^3 \\ a^3 & a^2 & 1 & a & a^7 & a^6 & a^5 & a^4 \\ a^4 & a^3 & a^2 & 1 & a & a^7 & a^6 & a^5 \\ a^5 & a^4 & a^3 & a^2 & 1 & a & a^7 & a^6 \\ a^6 & a^5 & a^4 & a^3 & a^2 & 1 & a & a^7 \\ a^7 & a^6 & a^5 & a^4 & a^3 & a^2 & 1 & a \\ a & a^7 & a^6 & a^5 & a^4 & a^3 & a^2 & 1 \end{bmatrix}$$

$$G_1^4 = \sum_R D^4(R)_{11} D(R) = 1 D(E) + a^3 D(R_1) + a^4 D(R_2) + a^5 D(R_3) + a^6 D(R_4) \\ + a^7 D(R_5) + a D(R_6) + a^2 D(R_7)$$

$$= \begin{bmatrix} 1 & a^2 & a & a^7 & a^6 & a^5 & a^4 & a^3 \\ a^3 & 1 & a^2 & a & a^7 & a^6 & a^5 & a^4 \\ a^4 & a^3 & 1 & a^2 & a & a^7 & a^6 & a^5 \\ a^5 & a^4 & a^3 & 1 & a^2 & a & a^7 & a^6 \\ a^6 & a^5 & a^4 & a^3 & 1 & a^2 & a & a^7 \\ a^7 & a^6 & a^5 & a^4 & a^3 & 1 & a^2 & a \\ a & a^7 & a^6 & a^5 & a^4 & a^3 & 1 & a^2 \\ a^2 & a & a^7 & a^6 & a^5 & a^4 & a^3 & 1 \end{bmatrix}$$

$$G_1^5 = \sum_R D^5(R)_{11} D(R) = 1 D(E) + a^4 D(R_1) + a^5 D(R_2) + a^6 D(R_3) + a^7 D(R_4) \\ + a D(R_5) + a^2 D(R_6) + a^3 D(R_7)$$

$$= \begin{bmatrix} 1 & a^3 & a^2 & a & a^7 & a^6 & a^5 & a^4 \\ a^4 & 1 & a^3 & a^2 & a & a^7 & a^6 & a^5 \\ a^5 & a^4 & 1 & a^3 & a^2 & a & a^7 & a^6 \\ a^6 & a^5 & a^4 & 1 & a^3 & a^2 & a & a^7 \\ a^7 & a^6 & a^5 & a^4 & 1 & a^3 & a^2 & a \\ a & a^7 & a^6 & a^5 & a^4 & 1 & a^3 & a^2 \\ a^2 & a & a^7 & a^6 & a^5 & a^4 & 1 & a^3 \\ a^3 & a^2 & a & a^7 & a^6 & a^5 & a^4 & 1 \end{bmatrix}$$

$$G_1^6 = \sum_R D^6(R)_{11} D(R) = 1 D(E) + a^5 D(R_1) + a^6 D(R_2) + a^7 D(R_3) + a D(R_4) \\ + a^2 D(R_5) + a^3 D(R_6) + a^4 D(R_7)$$

$$= \begin{bmatrix} 1 & a^4 & a^3 & a^2 & a & a^7 & a^6 & a^5 \\ a^5 & 1 & a^4 & a^3 & a^2 & a & a^7 & a^6 \\ a^6 & a^5 & 1 & a^4 & a^3 & a^2 & a & a^7 \\ a^7 & a^6 & a^5 & 1 & a^4 & a^3 & a^2 & a \\ a & a^7 & a^6 & a^5 & 1 & a^4 & a^3 & a^2 \\ a^2 & a & a^7 & a^6 & a^5 & 1 & a^4 & a^3 \\ a^3 & a^2 & a & a^7 & a^6 & a^5 & 1 & a^4 \\ a^4 & a^3 & a^2 & a & a^7 & a^6 & a^5 & 1 \end{bmatrix}$$

$$G_1^7 = \sum_R D^7(R)_{11} D(R) = 1 D(E) + a^6 D(R_1) + a^7 D(R_2) + a D(R_3) + a^2 D(R_4) \\ + a^3 D(R_5) + a^4 D(R_6) + a^5 D(R_7)$$

$$= \begin{bmatrix} 1 & a^5 & a^4 & a^3 & a^2 & a & a^7 & a^6 \\ a^6 & 1 & a^5 & a^4 & a^3 & a^2 & a & a^7 \\ a^7 & a^6 & 1 & a^5 & a^4 & a^3 & a^2 & a \\ a & a^7 & a^6 & 1 & a^5 & a^4 & a^3 & a^2 \\ a^2 & a & a^7 & a^6 & 1 & a^5 & a^4 & a^3 \\ a^3 & a^2 & a & a^7 & a^6 & 1 & a^5 & a^4 \\ a^4 & a^3 & a^2 & a & a^7 & a^6 & 1 & a^5 \\ a^5 & a^4 & a^3 & a^2 & a & a^7 & a^6 & 1 \end{bmatrix}$$

$$\text{and } G_1^8 = \sum_R D^8(R)_{11} D(R) = 1 D(E) + a^7 D(R_1) + a D(R_2) + a^2 D(R_3) + a^3 D(R_4) \\ + a^4 D(R_5) + a^5 D(R_6) + a^6 D(R_7)$$

$$= \begin{bmatrix} 1 & a^6 & a^5 & a^4 & a^3 & a^2 & a & a^7 \\ a^7 & 1 & a^6 & a^5 & a^4 & a^3 & a^2 & a \\ a & a^7 & 1 & a^6 & a^5 & a^4 & a^3 & a^2 \\ a^2 & a & a^7 & 1 & a^6 & a^5 & a^4 & a^3 \\ a^3 & a^2 & a & a^7 & 1 & a^6 & a^5 & a^4 \\ a^4 & a^3 & a^2 & a & a^7 & 1 & a^6 & a^5 \\ a^5 & a^4 & a^3 & a^2 & a & a^7 & 1 & a^6 \\ a^6 & a^5 & a^4 & a^3 & a^2 & a & a^7 & 1 \end{bmatrix}$$

Now, the basis vector α_{mnp} after normalization to unity will be as shown

$$\alpha_{111} = \frac{1}{\sqrt{8}} [1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1]^T$$

$$\alpha_{211} = \frac{1}{\sqrt{8}} [1 \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7]^T$$

$$\alpha_{311} = \frac{1}{\sqrt{8}} [1 \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a]^T$$

$$\alpha_{411} = \frac{1}{\sqrt{8}} [1 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a \ a^2]^T$$

$$\alpha_{511} = \frac{1}{\sqrt{8}} [1 \ a^4 \ a^5 \ a^6 \ a^7 \ a \ a^2 \ a^3]^T$$

$$\alpha_{611} = \frac{1}{\sqrt{8}} [1 \ a^5 \ a^6 \ a^7 \ a \ a^2 \ a^3 \ a^4]^T$$

$$\alpha_{711} = \frac{1}{\sqrt{8}} [1 \ a^6 \ a^7 \ a \ a^2 \ a^3 \ a^4 \ a^5]^T$$

and

$$\alpha_{811} = \frac{1}{\sqrt{8}} [1 \ a^7 \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6]^T$$

Thus the matrix $\alpha = A_c$ comes out to be

$$[A_c] = [\alpha_{111} \ \alpha_{211} \ \alpha_{311} \ \alpha_{411} \ \alpha_{511} \ \alpha_{611} \ \alpha_{711} \ \alpha_{811}]$$

$$D^1(R) \ D^2(R) \ D^3(R) \ D^4(R) \ D^5(R) \ D^6(R) \ D^7(R) \ D^8(R)$$

$$= \frac{1}{\sqrt{8}} \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 \\ 1 & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a \\ 1 & a^3 & a^4 & a^5 & a^6 & a^7 & a & a^2 \\ 1 & a^4 & a^5 & a^6 & a^7 & a & a^2 & a^3 \\ 1 & a^5 & a^6 & a^7 & a & a^2 & a^3 & a^4 \\ 1 & a^6 & a^7 & a & a^2 & a^3 & a^4 & a^5 \\ 1 & a^7 & a & a^2 & a^3 & a^4 & a^5 & a^6 \end{bmatrix} \quad (3.16)$$

We can see that this matrix is same as the one given in Eqn.(3.5).

It can be verified that $A_c^{*T} A_c = I$ hence $A_c^{-1} = A_c^{*T}$ i.e. A_c is unitary matrix. Now, from Eqn.(2.2)

$$\bar{v}_{pq}^{\text{phase}} = [Z_{pq}]^{\text{phase}} \bar{i}_{pq}^{\text{phase}}$$

We know that

$$\bar{v}_{pq}^{\text{phase}} = A_c \bar{v}_{pq}^{\text{comp.}} \quad \text{and} \quad \bar{i}_{pq}^{\text{phase}} = A_c \bar{i}_{pq}^{\text{comp.}}$$

So $A_c \bar{v}_{pq}^{\text{comp}} = [Z_{pq}]^{\text{phase}} A_c \bar{i}_{pq}^{\text{comp}}$

or $\bar{v}_{pq}^{\text{comp}} = A_c^{*T} [Z_{pq}]^{\text{phase}} A_c \bar{i}_{pq}^{\text{comp}} = [Z_{pq}]^{\text{comp}} \bar{i}_{pq}^{\text{comp}}$

Hence, $[Z_{pq}]^{\text{comp}} = A_c^{*T} [Z_{pq}]^{\text{phase}} A_c$ (3.17)

Substituting values of A_c^{*T} and A_c from eqn.(3.5) and $[Z_{pq}]^{\text{phase}}$ from eqn.(3.4) in eqn.(3.17), we get

$$[Z_{pq}]_{\text{comp}}^{0,1,2,3,4,5,6,7}$$

$$= \begin{bmatrix} z_{pq}^s + z_{pq}^{m1} + z_{pq}^{m2} + z_{pq}^{m3} + z_{pq}^{m4} + z_{pq}^{m5} + z_{pq}^{m6} + z_{pq}^{m7} \\ z_{pq}^s + a z_{pq}^{m1} + a^2 z_{pq}^{m2} - a^* z_{pq}^{m3} - z_{pq}^{m4} - a z_{pq}^{m5} - a^2 z_{pq}^{m6} + a^* z_{pq}^{m7} \\ \cdot \\ \cdot \\ \cdot \end{bmatrix} \quad (3.18)$$

Therefore,

$$z_{pq}^0 = z_{pq}^s + z_{pq}^{m1} + z_{pq}^{m2} + z_{pq}^{m3} + z_{pq}^{m4} + z_{pq}^{m5} + z_{pq}^{m6} + z_{pq}^{m7}$$

$$z_{pq}^1 = z_{pq}^s + a z_{pq}^{m1} + a^2 z_{pq}^{m2} - a^* z_{pq}^{m3} - z_{pq}^{m4} - a z_{pq}^{m5} - a^2 z_{pq}^{m6} + a^* z_{pq}^{m7}$$

and so on.

Here z_{pq}^0 is the zero sequence impedance and $z_{pq}^1, z_{pq}^2 \dots$ etc. are the first, second.... sequence impedances respectively.

Proposition: The transformation matrix A_c which diagonalizes the coefficient matrix of 8-phase rotating elements is a linear power invariant transformation matrix with complex elements similar to the symmetrical components.

3.2 8-PHASE STATIONARY ELEMENTS

In the previous chapter we have seen that 8-phase network which possesses reflection symmetries in addition to rotation symmetries, commonly known as stationary elements (typical example is that of 8-phase transposed transmission line) are symmetric under symmetry operations viz. $\sigma_8^1, \sigma_8^2, \sigma_8^3, \sigma_8^4, \sigma_8^5, \sigma_8^6, \sigma_8^7, E, \delta_a', \delta_b', \delta_c', \delta_d', \delta_e', \delta_f', \delta_g'$ and δ_h' . In the previous section we have seen that impedance matrix for a network possessing rotational symmetries is cyclic (Eqn.(3.4)). For the network possessing both rotational as well as reflection symmetries, applying Eqn.(3.1) for symmetry operation of reflection, we get for $R = \delta_a'$.

$$[Z_{pq}]^{abcdefgh} = D^{-1}(\delta_a') [Z_{pq}]^{abcdefgh} D(\delta_a')$$

We know that $D^{-1}(\delta_a') = D(\delta_a')$. Now substituting the values of $D(\delta_a')$ from Eqn.(2.6) and $[Z_{pq}]$ from Eqn.(3.4) and then comparing terms of matrices on the two sides, we get that $[Z_{pq}]$ is of the form:

$$[Z_{pq}]^{abcdefgh} = \begin{bmatrix} z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s \end{bmatrix} \quad (3.20)$$

As shown in Chapter 2, these sixteen symmetry operation form a group \mathcal{G}_v which are represented by permutation matrices given in equation (2.3) and equation (2.6). The order of the group \mathcal{G}_v is sixteen, but there are only seven classes viz.

$[D(E)]$, $[D(\mathcal{C}_8^1), D(\mathcal{C}_8^7)]$, $[D(\mathcal{C}_8^2), D(\mathcal{C}_8^6)]$, $[D(\mathcal{C}_8^3), D(\mathcal{C}_8^5)]$, $[D(\mathcal{C}_8^4)]$, $[D(\delta_a'), D(\delta_b'), D(\delta_c'), D(\delta_d')]$ and $[D(\delta_e'), D(\delta_f'), D(\delta_g'), D(\delta_h')]$. Therefore, the number of irreducible representations is also seven. Let $l_1, l_2, l_3, l_4, l_5, l_6$ and l_7 be the dimensions of these irreducible representations. Then from Eqn.(3.7), we have

$$\sum_{i=1}^7 l_i^2 = l_1^2 + l_2^2 + \dots + l_7^2 = h = 16$$

The solution of this equation is $l_1 = l_2 = l_3 = l_4 = 1$ and $l_5 = l_6 = l_7 = 2$. From this we conclude that there are four irreducible representations viz. $D^1(R)$, $D^2(R)$, $D^3(R)$ and

$D^4(R)$ of dimension 1 each and three irreducible representations viz. $D^5(R)$, $D^6(R)$ and $D^7(R)$ of dimension 2 each. Since, from equation (3.8)

$$\sum_R \chi_i^2(R) = h = 16$$

the characters of each of sixteen elements of the first four irreducible representations whose dimension is 1, is 1 or -1, but that of the last three representations whose dimension is 2, is 2, -2 or 0. Hence the character table is

C_{8v}	E	C_8^1	C_8^2	C_8^3	C_8^4	C_8^5	C_8^6	C_8^7	δ'_a	δ'_b	δ'_c	δ'_d	δ'_e	δ'_f	δ'_g	δ'_h
$X^1(R)$	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
$X^2(R)$	1	1	1	1	1	1	1	1	-1	-1	-1	-1	-1	-1	-1	-1
$X^3(R)$	1	-1	1	-1	1	-1	1	-1	1	1	1	1	-1	-1	-1	-1
$X^4(R)$	1	-1	1	-1	1	-1	1	-1	-1	-1	-1	-1	1	1	1	1
$X^5(R)$	2	0	-2	0	-2	0	2	0	0	0	0	0	0	0	0	0
$X^6(R)$	2	0	2	0	-2	0	-2	0	0	0	0	0	0	0	0	0
$X^7(R)$	2	0	-2	0	2	0	-2	0	0	0	0	0	0	0	0	0
Red.Rep.																
$X(R)$	8	0	0	0	0	0	0	0	2	2	2	2	0	0	0	0

(3.21)

It is evident that the irreducible representations of $D^1(R)$, $D^2(R)$, $D^3(R)$ and $D^4(R)$ whose dimensions are 1, are the same as their characters but $D^5(R)$, $D^6(R)$ and $D^7(R)$ are not. Using the orthogonality theorem (Appendix 2) and its consequences the irreducible representation of the group comes out to be:

The number of times the irreducible representations $D^i(R)$ appear at the diagonal of $\bar{D}(R)$ is determined as follows:

$$1 \leftarrow 1(1) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) = 1$$

0)

1) = 0

E	C_i
1	1
1	1
1	-1
1	-1
$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$	$\begin{bmatrix} 0 \\ -1 \end{bmatrix}$
$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$	$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$
$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$	$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$

The number of times the irreducible representations $D^i(R)$ appear at the diagonal of $\bar{D}(R)$ is determined as follows:

$$a_1 = \frac{1}{h} \sum_R X^1(R) X(R) = \frac{1}{16} (1(8) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(2) + 1(2) + 1(2) + 1(2) + 1(0) + 1(0) + 1(0) + 1(0)) = 1$$

$$a_2 = \frac{1}{h} \sum_R X^2(R) X(R) = \frac{1}{16} (1(8) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) + 1(0) - 1(2) - 1(2) - 1(2) - 1(2) - 1(0) - 1(0) - 1(0) - 1(0)) = 0$$

Similarly

$$a_3 = \frac{1}{h} \sum_R X^3(R) X(R) = \frac{1}{16} (1(8) + 1(2) + 1(2) + 1(2) + 1(2)) = 1$$

$$a_4 = \frac{1}{h} \sum_R X^4(R) X(R) = \frac{1}{16} (1(8) - 1(2) - 1(2) - 1(2) - 1(2)) = 0$$

$$a_5 = \frac{1}{h} \sum_R X^5(R) X(R) = \frac{1}{16} (2(8) + 0) = 1$$

$$a_6 = \frac{1}{h} \sum_R X^6(R) X(R) = \frac{1}{16} (2(8) + 0) = 1$$

$$a_7 = \frac{1}{h} \sum_R X^7(R) X(R) = \frac{1}{16} (2(8) + 0) = 1$$

Let transformation matrix α be designated by A_r , then

$$\bar{D}(R) = A_r^{*T} D(R) A_r = \begin{bmatrix} D^1(R) & & & & & & \\ & D^3(R) & & & & & \\ & & D^5(R) & & & & \\ & & & D^6(R) & & & \\ & & & & D^7(R) & & \\ & & & & & & \\ & & & & & & \end{bmatrix} \quad (3.23)$$

Now we determine the matrix G_i^j (following the same procedure as in previous section) as follows:

$$\begin{aligned}
 G_1^1 &= \sum_R D^1(R)_{11} D(R) \quad \text{for } R = E, C_8^1, C_8^2, \dots, C_8^7 \text{ and } \delta_a^1, \delta_b^1, \dots, \delta_h^1 \\
 &= 1D(E) + 1D(C_8^1) + 1D(C_8^2) + 1D(C_8^3) + 1D(C_8^4) + 1D(C_8^5) + 1D(C_8^6) + 1D(C_8^7) + 1D(\delta_a^1) \\
 &\quad + 1D(\delta_b^1) + 1D(\delta_c^1) + 1D(\delta_d^1) + 1D(\delta_e^1) + 1D(\delta_f^1) + 1D(\delta_g^1) + 1D(\delta_h^1)
 \end{aligned}$$

$$= \begin{bmatrix} 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \end{bmatrix}$$

$$\begin{aligned}
 G_1^2 &= \sum_R D^2(R)_{11} D(R) = 1D(E) + 1D(C_8^1) + 1D(C_8^2) + 1D(C_8^3) + 1D(C_8^4) + 1D(C_8^5) \\
 &\quad + 1D(C_8^6) + 1D(C_8^7) - 1D(\delta_a^1) - 1D(\delta_b^1) - 1D(\delta_c^1) - 1D(\delta_d^1) \\
 &\quad - 1D(\delta_e^1) - 1D(\delta_f^1) - 1D(\delta_g^1) - 1D(\delta_h^1) = [0]
 \end{aligned}$$

$$\begin{aligned}
 G_1^3 &= \sum_R D^3(R)_{11} D(R) = 1D(E) - 1D(C_8^1) + 1D(C_8^2) - 1D(C_8^3) + 1D(C_8^4) - 1D(C_8^5) \\
 &\quad + 1D(C_8^6) - 1D(C_8^7) + 1D(\delta_a^1) + 1D(\delta_b^1) + 1D(\delta_c^1) + 1D(\delta_d^1) \\
 &\quad - 1D(\delta_e^1) - 1D(\delta_f^1) - 1D(\delta_g^1) - 1D(\delta_h^1)
 \end{aligned}$$

$$= \begin{bmatrix} 2 & -2 & 2 & -2 & 2 & -2 & 2 & -2 \\ -2 & 2 & -2 & 2 & -2 & 2 & -2 & 2 \\ 2 & -2 & 2 & -2 & 2 & -2 & 2 & -2 \\ -2 & 2 & -2 & 2 & -2 & 2 & -2 & 2 \\ 2 & -2 & 2 & -2 & 2 & -2 & 2 & -2 \\ -2 & 2 & -2 & 2 & -2 & 2 & -2 & 2 \\ 2 & -2 & 2 & -2 & 2 & -2 & 2 & -2 \\ -2 & 2 & -2 & 2 & -2 & 2 & -2 & 2 \end{bmatrix}$$

$$G_1^4 = \sum_R D^4(R)_{11} D(R) = 1D(E) - 1D(C_8^1) + 1D(C_8^2) - 1D(C_8^3) + 1D(C_8^4) - 1D(C_8^5) \\ + 1D(C_8^6) - 1D(C_8^7) - 1D(\delta_a') - 1D(\delta_b') - 1D(\delta_c') - 1D(\delta_d') \\ + 1D(\delta_e') + 1D(\delta_f') + 1D(\delta_g') + 1D(\delta_h') = [0]$$

$$G_1^5 = \sum_R D^5(R)_{11} D(R) = 1D(E) - 1D(C_8^2) - 1D(C_8^4) + 1D(C_8^6) + 1D(\delta_a') + 1D(\delta_b') \\ - 1D(\delta_c') - 1D(\delta_d')$$

$$= \begin{bmatrix} 2 & 0 & 2 & 0 & -2 & 0 & -2 & 0 \\ 0 & 2 & 0 & 0 & 0 & -2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -2 & 0 & 0 & 0 & 2 & 0 & 0 \\ -2 & 0 & -2 & 0 & 2 & 0 & 2 & 0 \\ 0 & -2 & 0 & 0 & 0 & 2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 2 & 0 & 0 & 0 & -2 & 0 & 0 \end{bmatrix}$$

$$G_2^5 = \sum_R D^5(R)_{22} D(R)$$

$$= 1D(E) - 1D(C_8^2) - 1D(C_8^4) + 1D(C_8^6) - 1D(\delta_a') - 1D(\delta_b') + 1D(\delta_c') + 1D(\delta_d')$$

$$= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 2 & 0 & 0 & 0 & -2 \\ -2 & 0 & 2 & 0 & 2 & 0 & -2 & 0 \\ 0 & 0 & 0 & 2 & 0 & 0 & 0 & -2 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -2 & 0 & 0 & 0 & 2 \\ 2 & 0 & -2 & 0 & -2 & 0 & 2 & 0 \\ 0 & 0 & 0 & -2 & 0 & 0 & 0 & 2 \end{bmatrix}$$

$$G_1^6 = \sum_R D^6(R)_{11} D(R)$$

$$= 1D(E) + 1D(C_8^2) - 1D(C_8^4) - 1D(C_8^6) + 1D(\delta'_e) + 1D(\delta'_f) - 1D(\delta'_g) - 1D(\delta'_h)$$

$$= \begin{bmatrix} 1 & 1 & -1 & 1 & -1 & -1 & 1 & -1 \\ 1 & 1 & 1 & -1 & -1 & -1 & -1 & 1 \\ 1 & 1 & 1 & -1 & -1 & -1 & -1 & 1 \\ 1 & 1 & -1 & 1 & -1 & -1 & 1 & -1 \\ -1 & -1 & 1 & -1 & 1 & 1 & -1 & 1 \\ -1 & -1 & -1 & 1 & 1 & 1 & 1 & -1 \\ -1 & -1 & -1 & 1 & 1 & 1 & 1 & -1 \\ -1 & -1 & 1 & -1 & 1 & 1 & -1 & 1 \end{bmatrix}$$

$$G_2^6 = \sum_R D^6(R)_{22} D(R)$$

$$= 1D(E) + 1D(C_8^2) - 1D(C_8^4) - 1D(C_8^6) - 1D(\delta'_e) - 1D(\delta'_f) + 1D(\delta'_g) + 1D(\delta'_h)$$

$$= \begin{bmatrix} 0 & -1 & 0 & 1 & 0 & -1 & 0 & 1 \\ -1 & 2 & 1 & -2 & -1 & 2 & 1 & -2 \\ 0 & 1 & 0 & -1 & 0 & 1 & 0 & -1 \\ 1 & -2 & -1 & 2 & 1 & -2 & -1 & 2 \\ 0 & -1 & 0 & 1 & 0 & -1 & 0 & 1 \\ -1 & 2 & 1 & -2 & -1 & 2 & 1 & -2 \\ 0 & 1 & 0 & -1 & 0 & 1 & 0 & -1 \\ 1 & -2 & -1 & 2 & 1 & -2 & -1 & 2 \end{bmatrix}$$

The basis vector α_{mnp} after normalization to unity comes out to be

$$\alpha_{111} = \frac{1}{\sqrt{8}} [1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1]^T$$

$$\alpha_{311} = \frac{1}{\sqrt{8}} [1 \ -1 \ 1 \ -1 \ 1 \ -1 \ 1 \ -1]^T$$

$$\alpha_{511} = \frac{1}{\sqrt{8}} [2 \ 0 \ 0 \ 0 \ -2 \ 0 \ 0 \ 0]^T$$

$$\alpha_{521} = \frac{1}{\sqrt{8}} [0 \ 0 \ -2 \ 0 \ 0 \ 0 \ 2 \ 0]^T$$

$$\alpha_{611} = \frac{1}{\sqrt{8}} [1 \ 1 \ 1 \ 1 \ -1 \ -1 \ -1 \ -1]^T$$

$$\alpha_{621} = \frac{1}{\sqrt{8}} [1 \ -1 \ 1 \ -1 \ -1 \ 1 \ -1 \ 1]^T$$

$$\alpha_{711} = \frac{1}{\sqrt{8}} [\sqrt{2} \ 0 \ -\sqrt{2} \ 0 \ \sqrt{2} \ 0 \ -\sqrt{2} \ 0]^T$$

$$\alpha_{721} = \frac{1}{\sqrt{8}} [0 \ -\sqrt{2} \ 0 \ \sqrt{2} \ 0 \ -\sqrt{2} \ 0 \ \sqrt{2}]^T$$

Therefore, the matrix $\alpha = A_r$

$$\begin{aligned}
 &= \begin{matrix} \alpha_{111} & \alpha_{311} & \alpha_{511} & \alpha_{521} & \alpha_{611} & \alpha_{621} & \alpha_{711} & \alpha_{721} \\ D^1(R) & D^3(R) & D^5(R) & & D^6(R) & & D^7(R) & \end{matrix} \\
 &= \frac{1}{\sqrt{8}} \begin{bmatrix} 1 & 1 & 2 & 0 & 1 & 1 & \sqrt{2} & 0 \\ 1 & -1 & 0 & 0 & 1 & -1 & 0 & -\sqrt{2} \\ 1 & 1 & 0 & -2 & 1 & 1 & -\sqrt{2} & 0 \\ 1 & -1 & 0 & 0 & 1 & -1 & 0 & \sqrt{2} \\ 1 & 1 & -2 & 0 & -1 & -1 & \sqrt{2} & 0 \\ 1 & -1 & 0 & 0 & -1 & 1 & 0 & -\sqrt{2} \\ 1 & 1 & 0 & 2 & -1 & -1 & -\sqrt{2} & 0 \\ 1 & -1 & 0 & 0 & -1 & 1 & 0 & \sqrt{2} \end{bmatrix} \quad (3.24)
 \end{aligned}$$

It can be verified that $A_r^T A_r = I = A_r^{-1} A_r$, and therefore the transformation matrix A_r is orthogonal. Now, from Eqn. (3.17)

$$[Z_{pq}]_{\text{comp}}^{0,1,2,3,4,5,6,7} = A_r^T [Z_{pq}]_{\text{phase}}^{\text{abcdefgh}} A_r$$

Substituting values for A_r and $[Z_{pq}]_{\text{phase}}$ from Eqn. (3.24) and (3.20) respectively, we get the impedance matrix in the component form:

$$[Z_{pq}]_{\text{comp}}^{0,1,2,3,4,5,6,7} = \begin{bmatrix} z_{pq}^s + 7z_{pq}^m & & & & & & & \\ & z_{pq}^s - z_{pq}^m & & & & & & 0 \\ & & z_{pq}^s - z_{pq}^m & & & & & \\ & & & z_{pq}^s - z_{pq}^m & & & & \\ & & & & z_{pq}^s - z_{pq}^m & & & \\ & & & & & z_{pq}^s - z_{pq}^m & & \\ & & & & & & z_{pq}^s - z_{pq}^m & \\ 0 & & & & & & & z_{pq}^s - z_{pq}^m \\ & & & & & & & & z_{pq}^s - z_{pq}^m \end{bmatrix} \quad (3.25)$$

From this it is clear that the transformation matrix A_r diagonalizes the coefficient matrix $[Z_{pq}]$ of 8-phase stationary elements. It is to be noted here that the matrix A_c derived earlier can also diagonalize $[Z_{pq}]$ since stationary elements also possess rotational symmetries in addition to reflection ones. The diagonal elements of $[Z_{pq}]_{\text{comp}}$ are the sequence impedances in this case, more specifically, the zero sequence impedance $z_{pq}^0 = z_{pq}^s + 7z_{pq}^m$ and 1st, 2nd, 3rd, 4th, 5th, 6th and 7th sequence impedances are all equal to $z_{pq}^s - z_{pq}^m$.

Complex Power

The complex power in the 8-phase stationary element p-q

$$S_{pq} = P_{pq} - jQ_{pq} = \bar{v}_{pq}^{abcdefgh} *^T \bar{i}_{pq}^{abcdefgh}$$

$$\begin{aligned}
&= [A_r \bar{v}_{pq}^{0,1,2,3,4,5,6,7}]^{*T} [A_r \bar{i}_{pq}^{0,1,2,3,4,5,6,7}] \\
&= [\bar{v}_{pq}^{0,1,2,3,4,5,6,7}]^{*T} A_r^{*T} A_r [\bar{i}_{pq}^{0,1,2,3,4,5,6,7}] \\
&= [\bar{v}_{pq}^{0,1,2,3,4,5,6,7}]^{*T} [\bar{i}_{pq}^{0,1,2,3,4,5,6,7}] \\
&\quad \text{as } A_r^* = A_r \text{ and } A_r^{*T} A_r = A_r^T A_r = I
\end{aligned}$$

Hence we conclude:

Proposition: The orthogonal matrix A_r which transforms the field of phasors of a 8-phase system to the field of components is a linear power invariant real transformation matrix similar to Clarke's component transformation matrix of 3-phase systems.

CHAPTER 4

12-PHASE POWER SYSTEM NETWORKS

In the previous chapter, we derived suitable transformations for the purpose of both steady state as well as transient analysis of 8-phase systems. Here, we derive the transformations for the analysis of 12-phase systems and also the expression for sequence impedances and complex power.

4.1 12-PHASE ROTATING ELEMENTS

For rotating elements, the symmetries are such that circularly permuting port voltages will cause similar permutations of the port currents, i.e., if the voltage vector $\bar{v}_{pq}^{\text{phase}}$ is changed to $D(R) \bar{v}_{pq}^{\text{phase}}$ then correspondingly the current vector $\bar{i}_{pq}^{\text{phase}}$ is replaced by $D(R) \bar{i}_{pq}^{\text{phase}}$. So

$$D(R) \bar{v}_{pq}^{\text{phase}} = [Z_{pq}]_{\text{phase}} D(R) \bar{i}_{pq}^{\text{phase}}$$

$$\text{or} \quad \bar{v}_{pq}^{\text{phase}} = D^{-1}(R) [Z_{pq}]_{\text{phase}} D(R) \bar{i}_{pq}^{\text{phase}} \quad (4.1)$$

Comparing equation (2.4) and equation (4.1) we get

$$[Z_{pq}]_{\text{phase}} = D^{-1}(R) [Z_{pq}]_{\text{phase}} D(R)$$

Taking $R = J_{12}^1$, then $D^{-1}(J_{12}^1) = D(J_{12}^{11})$

$$[Z_{pq}]_{\text{phase}} = D(J_{12}^{11}) [Z_{pq}]_{\text{phase}} D(J_{12}^1) \quad (4.2)$$

Performing the matrix multiplications and then making term by term comparison in Eqn.(4.2), we find that Z_{pq} phase is cyclic matrix and is of the form: $Z_{pq} \text{ phase} =$

z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}
z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}
z_{pq}^{10}	z_{pq}^{11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}
z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}
z_{pq}^8	z_{pq}^9	z_{pq}^{10}	z_{pq}^{11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}
z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}
z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}
z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}
z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}
z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}	z_{pq}^{m2}
z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s	z_{pq}^{m1}
z_{pq}^{m1}	z_{pq}^{m2}	z_{pq}^{m3}	z_{pq}^{m4}	z_{pq}^{m5}	z_{pq}^{m6}	z_{pq}^{m7}	z_{pq}^{m8}	z_{pq}^{m9}	z_{pq}^{m10}	z_{pq}^{m11}	z_{pq}^s

Now, the eigenvectors of permutation matrices (equation 2.5) given by the following matrix A_c [11]

$$A_c = \frac{1}{\sqrt{12}} \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} \\ 1 & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a \\ 1 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 \\ 1 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 \\ 1 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 \\ 1 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 \\ 1 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 \\ 1 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 \\ 1 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 \\ 1 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 \\ 1 & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} \end{bmatrix}$$

Matrix A_c can also be expressed as

$$A_c = \frac{1}{\sqrt{12}} \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a & a^2 & a^3 & -a^{*2} & -a^{*} & -1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} \\ 1 & a^2 & a^3 & -a^{*2} & -a^{*} & -1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} & a \\ 1 & a^3 & -a^{*2} & -a^{*} & -1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} & a & a^2 \\ 1 & -a^{*2} & -a^{*} & -1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} & a & a^2 & a^3 \\ 1 & -a^{*} & -1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} & a & a^2 & a^3 & -a^{*2} \\ 1 & -1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} & a & a^2 & a^3 & -a^{*2} & -a^{*} \\ 1 & -a & -a^2 & -a^3 & a^{*2} & a^{*} & a & a^2 & a^3 & -a^{*2} & -a^{*} & -1 \\ 1 & -a^2 & -a^3 & a^{*2} & a^{*} & a & a^2 & a^3 & -a^{*2} & -a^{*} & -1 & -a \\ 1 & -a^3 & a^{*2} & a^{*} & a & a^2 & a^3 & -a^{*2} & -a^{*} & -1 & -a & -a^2 \\ 1 & a^{*2} & a^{*} & a & a^2 & a^3 & -a^{*2} & -a^{*} & -1 & -a & -a^2 & -a^3 \\ 1 & a^{*} & a & a^2 & a^3 & -a^{*2} & -a^{*} & -1 & -a & -a^2 & -a^3 & a^{*2} \end{bmatrix}$$

$$\text{because } a = e^{j2\pi/12} = 1\angle 30^\circ = \frac{1}{2}(\sqrt{3} + j1)$$

$$a^2 = e^{j4\pi/12} = 1\angle 60^\circ = \frac{1}{2}(1 + j\sqrt{3})$$

$$a^3 = e^{j6\pi/12} = 1\angle 90^\circ = j$$

$$a^4 = e^{j8\pi/12} = 1\angle 120^\circ = \frac{1}{2}(-1 + j\sqrt{3}) = -a^{*2}$$

$$a^5 = e^{j10\pi/12} = 1\angle 150^\circ = \frac{1}{2}(-\sqrt{3} + j1) = -a^*$$

$$a^6 = e^{j12\pi/12} = 1\angle 180^\circ = -1$$

$$a^7 = -a ; \quad a^8 = -a^2 ; \quad a^9 = a^{*3} ; \quad a^{10} = a^{*2},$$

$$a^{11} = a^* ; \quad a^{12} = 1$$

The unitary matrix A_c which diagonalizes the permutation matrix $D(R)$, will also diagonalize the impedance matrix $[Z_{pq}]$ if it commutes with $D(R)$. The matrix A_c is the transformation matrix for 12-phase power system network similar to symmetrical component matrix for a 3-phase system.

Now, we rederive the transformation matrix A_c , using group theoretic techniques, for 12-phase system.

Group Theoretic Approach:

We have seen in Chapter 2 that permutation matrices (equation 2.5) representing rotational symmetries of a 12-phase power system network form a cyclic group G_{12} of order 12. Each element of group is in a separate class. Therefore, the number of classes in group G_{12} will be equal to 12 and the number of

irreducible representations which are equal to the number of classes will also be equal to 12. Let l_1, l_2, \dots, l_{12} be the dimensions of these irreducible representations, then from Eqn. (3.7), we get

$$\sum_{i=1}^{12} l_i^2 = l_1^2 + l_2^2 + \dots + l_{12}^2 = 12$$

i.e. $l_1 = l_2 = \dots = l_{12} = 1$

Therefore all the irreducible representations have the dimension equal to 1. Likewise from equation (3.8) $\sum_{i=1}^{12} X_i^2(R) = 12$ and hence the characters $X_i(R)$ are each of unity modulus. Using standard computational techniques based on the orthogonality theorem (Appendix 2), one gets the character table shown below:

\mathcal{C}_{12}	E	\mathcal{C}_{12}^1	\mathcal{C}_{12}^2	\mathcal{C}_{12}^3	\mathcal{C}_{12}^4	\mathcal{C}_{12}^5	\mathcal{C}_{12}^6	\mathcal{C}_{12}^7	\mathcal{C}_{12}^8	\mathcal{C}_{12}^9	\mathcal{C}_{12}^{10}	\mathcal{C}_{12}^{11}
$X^1(R)$	1	1	1	1	1	1	1	1	1	1	1	1
$X^2(R)$	1	a	a ²	a ³	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹
$X^3(R)$	1	a ²	a ³	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹	a
$X^4(R)$	1	a ³	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹	a	a ²
$X^5(R)$	1	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹	a	a ²	a ³
$X^6(R)$	1	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹	a	a ²	a ³	a ⁴
$X^7(R)$	1	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹	a	a ²	a ³	a ⁴	a ⁵
$X^8(R)$	1	a ⁷	a ⁸	a ⁹	a ¹⁰	a ¹¹	a	a ²	a ³	a ⁴	a ⁵	a ⁶
$X^9(R)$	1	a ⁸	a ⁹	a ¹⁰	a ¹¹	a	a ²	a ³	a ⁴	a ⁵	a ⁶	a ⁷
$X^{10}(R)$	1	a ⁹	a ¹⁰	a ¹¹	a	a ²	a ³	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸
$X^{11}(R)$	1	a ¹⁰	a ¹¹	a	a ²	a ³	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹
$X^{12}(R)$	1	a ¹¹	a	a ²	a ³	a ⁴	a ⁵	a ⁶	a ⁷	a ⁸	a ⁹	a ¹⁰

Similarly, $a_2 = a_3 = a_4 = a_5 = a_6 = a_7 = a_8 = a_9 = a_{10} = a_{11}$
 $= a_{12} = 1$

Therefore $\bar{D}(R)$ is of the form:

$$\bar{D}(R) = \begin{bmatrix} D^1(R) & & & & & & & & & & & \\ & D^2(R) & & & & & 0 & & & & & \\ & & D^3(R) & & & & & & & & & \\ & & & D^4(R) & & & & & & & & \\ & & & & D^5(R) & & & & & & & \\ & & & & & D^6(R) & & & & & & \\ & & & & & & D^7(R) & & & & & \\ & & & & & & & D^8(R) & & & & \\ & & & & & & & & D^9(R) & & & \\ & & & & & & & & & D^{10}(R) & & \\ & & & & & & & & & & D^{11}(R) & \\ & 0 & & & & & & & & & & D^{12}(R) \end{bmatrix} \quad (4.7)$$

Now, we construct the matrices G_i^j using Eqn.(3.16), i.e.

$$G_i^j = \sum_R D^j(R)_{ii} D(R) \quad \text{for } j = 1, 2, \dots, 12$$

$$G_1^1 = \sum_R D^1(R)_{11} D(R) = 1D(E) + 1D(R_1) + 1D(R_2) + 1D(R_3) + 1D(R_4) + 1D(R_5) \\ + 1D(R_6) + 1D(R_7) + 1D(R_8) + 1D(R_9) + 1D(R_{10}) + 1D(R_{11}) + 1D(R_{12})$$

where $R_i = \mathcal{U}_{12}^i$ for $i = 1, 2, \dots, 11$.

$$G_1^2 = \sum_R D^2(R)_{11} D(R) = 1D(E) + aD(R_1) + a^2D(R_2) + a^3D(R_3) + a^4D(R_4) + a^5D(R_5) \\ + a^6D(R_6) + a^7D(R_7) + a^8D(R_8) + a^9D(R_9) + a^{10}D(R_{10}) + a^{11}D(R_{11}) + a^{12}D(R_{12})$$

$$G_1^3 = \sum_R D^3(R)_{11} D(R) = 1D(E) + a^2 D(R_1) + a^3 D(R_2) + a^4 D(R_3) + a^5 D(R_4) + a^6 D(R_5) \\ + a^7 D(R_6) + a^8 D(R_7) + a^9 D(R_8) + a^{10} D(R_9) + a^{11} D(R_{10}) \\ + a D(R_{11}),$$

$$G_1^4 = \sum_R D^4(R)_{11} D(R) = 1D(E) + a^3 D(R_1) + a^4 D(R_2) + a^5 D(R_3) + a^6 D(R_4) + a^7 D(R_5) \\ + a^8 D(R_6) + a^9 D(R_7) + a^{10} D(R_8) + a^{11} D(R_9) + a D(R_{10}) \\ + a^2 D(R_{11}),$$

$$G_1^5 = \sum_R D^5(R)_{11} D(R) = 1D(E) + a^4 D(R_1) + a^5 D(R_2) + a^6 D(R_3) + a^7 D(R_4) + a^8 D(R_5) \\ + a^9 D(R_6) + a^{10} D(R_7) + a^{11} D(R_8) + a D(R_9) + a^2 D(R_{10}) \\ + a^3 D(R_{11}),$$

$$G_1^6 = \sum_R D^6(R)_{11} D(R) = 1D(E) + a^5 D(R_1) + a^6 D(R_2) + a^7 D(R_3) + a^8 D(R_4) + a^9 D(R_5) \\ + a^{10} D(R_6) + a^{11} D(R_7) + a D(R_8) + a^2 D(R_9) + a^3 D(R_{10}) \\ + a^4 D(R_{11}),$$

$$G_1^7 = \sum_R D^7(R)_{11} D(R) = 1D(E) + a^6 D(R_1) + a^7 D(R_2) + a^8 D(R_3) + a^9 D(R_4) + a^{10} D(R_5) \\ + a^{11} D(R_6) + a D(R_7) + a D(R_8) + a^3 D(R_9) + a^4 D(R_{10}) \\ + a^5 D(R_{11}),$$

$$G_1^8 = \sum_R D^8(R)_{11} D(R) = 1D(E) + a^7 D(R_1) + a^8 D(R_2) + a^9 D(R_3) + a^{10} D(R_4) \\ + a^{11} D(R_5) + a D(R_6) + a^2 D(R_7) + a^3 D(R_8) + a^4 D(R_9) \\ + a^5 D(R_{10}) + a^6 D(R_{11}),$$

$$G_1^9 = \sum_R D^9(R)_{11} D(R) = 1D(E) + a^8 D(R_1) + a^9 D(R_2) + a^{10} D(R_3) + a^{11} D(R_4) \\ + a D(R_5) + a^2 D(R_6) + a^3 D(R_7) + a^4 D(R_8) + a^5 D(R_9) \\ + a^6 D(R_{10}) + a^7 D(R_{11}),$$

$$G_1^{10} = \sum_R D^{10}(R)_{11} D(R) = 1D(E) + a^9 D(R_1) + a^{10} D(R_2) + a^{11} D(R_3) + a D(R_4) \\ + a^2 D(R_5) + a^3 D(R_6) + a^4 D(R_7) + a^5 D(R_8) + a^6 D(R_9) \\ + a^7 D(R_{10}) + a^8 D(R_{11}),$$

$$G_1^{11} = \sum_R D^{11}(R)_{11} D(R) = 1D(E) + a^{10} D(R_1) + a^{11} D(R_2) + a D(R_3) + a^2 D(R_4) \\ + a^3 D(R_5) + a^4 D(R_6) + a^5 D(R_7) + a^6 D(R_8) + a^7 D(R_9) \\ + a^8 D(R_{10}) + a^9 D(R_{11}),$$

and

$$G_1^{12} = \sum_R D^{12}(R)_{11} D(R) = 1D(E) + a^{11} D(R_1) + a D(R_2) + a^2 D(R_3) + a^3 D(R_4) \\ + a^4 D(R_5) + a^5 D(R_6) + a^6 D(R_7) + a^7 D(R_8) + a^8 D(R_9) \\ + a^9 D(R_{10}) + a^{10} D(R_{11}).$$

Now, scanning the matrices \mathcal{A}_i^j 's from left to right and picking first linearly independent columns from each of these matrices we get the basis vector α_{mnp} . The basis vectors after normalization to unity come out to be

$$\alpha_{111} = \frac{1}{\sqrt{12}} [1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1]^T$$

$$\alpha_{211} = \frac{1}{\sqrt{12}} [1 \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11}]^T$$

$$\alpha_{311} = \frac{1}{\sqrt{12}} [1 \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a]^T$$

$$\alpha_{411} = \frac{1}{\sqrt{12}} [1 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a \ a^2]^T$$

$$\alpha_{511} = \frac{1}{\sqrt{12}} [1 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a \ a^2 \ a^3]^T$$

$$\alpha_{611} = \frac{1}{\sqrt{12}} [1 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a \ a^2 \ a^3 \ a^4]^T$$

$$\alpha_{711} = \frac{1}{\sqrt{12}} [1 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a \ a^2 \ a^3 \ a^4 \ a^5]^T$$

$$\alpha_{811} = \frac{1}{\sqrt{12}} [1 \ a^7 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6]^T$$

$$\alpha_{911} = \frac{1}{\sqrt{12}} [1 \ a^8 \ a^9 \ a^{10} \ a^{11} \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7]^T$$

$$\alpha_{10 \ 11} = \frac{1}{\sqrt{12}} [1 \ a^9 \ a^{10} \ a^{11} \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8]^T$$

$$\alpha_{11 \ 11} = \frac{1}{\sqrt{12}} [1 \ a^{10} \ a^{11} \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9]^T$$

$$\alpha_{12 \ 11} = \frac{1}{\sqrt{12}} [1 \ a^{11} \ a \ a^2 \ a^3 \ a^4 \ a^5 \ a^6 \ a^7 \ a^8 \ a^9 \ a^{10}]^T$$

Thus the transformation matrix $A_c = \alpha$ comes out to be

$$\alpha_{111} \ \alpha_{211} \ \alpha_{311} \ \alpha_{411} \ \alpha_{511} \ \alpha_{611} \ \alpha_{711} \ \alpha_{811}$$

$$D^1(R) \ D^2(R) \ D^3(R) \ D^4(R) \ D^5(R) \ D^6(R) \ D^7(R) \ D^8(R)$$

$$A_c =$$

$$\alpha_{911} \ \alpha_{10 \ 11} \ \alpha_{11 \ 11} \ \alpha_{12 \ 11}$$

$$D^9(R) \ D^{10}(R) \ D^{11}(R) \ D^{12}(R)$$

$$A_c = \frac{1}{\sqrt{12}} \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} \\ 1 & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a \\ 1 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 \\ 1 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 \\ 1 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 \\ 1 & a^6 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 \\ 1 & a^7 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 \\ 1 & a^8 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 \\ 1 & a^9 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 \\ 1 & a^{10} & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 \\ 1 & a^{11} & a & a^2 & a^3 & a^4 & a^5 & a^6 & a^7 & a^8 & a^9 & a^{10} \end{bmatrix} \quad (4.8)$$

We can see that this matrix is same as the one given in Eqn.(4

It can be seen that $A_c^{*T} A_c = I$ i.e. A_c is unitary and power invariant. Now from Eqn.(3.17),

$$[Z_{pq}]_{\text{comp}} = A_c^{*T} [Z_{pq}]_{\text{phase}} A_c$$

Substituting for A_c from eqn.(4.4) and $[Z_{pq}]_{\text{phase}}$ from (4.3), we get

$$Z_{pq \text{ comp}}^{0,1,2,3,4,5,6,7,8,9,10,11} =$$

$$\begin{aligned} & z_{pq}^s + z_{pq}^{m1} + z_{pq}^{m2} + z_{pq}^{m3} + z_{pq}^{m4} + z_{pq}^{m5} + z_{pq}^{m6} + z_{pq}^{m7} + z_{pq}^{m8} + z_{pq}^{m9} + z_{pq}^{m10} + z_{pq}^{m11} & 0 \\ & z_{pq}^s + az_{pq}^{m1} + a^2 z_{pq}^{m2} + a^3 z_{pq}^{m3} - a^* z_{pq}^{m4} - a^* z_{pq}^{m5} - z_{pq}^{m6} - az_{pq}^{m7} - a^2 z_{pq}^{m8} \\ & a^3 z_{pq}^{m9} + a^* z_{pq}^{m10} + a^* z_{pq}^{m11} \end{aligned}$$

Therefore, the zero sequence impedance z_{pq}^0 is equal to

$$z_{pq}^0 = z_{pq}^s + z_{pq}^{m1} + z_{pq}^{m2} + z_{pq}^{m3} + z_{pq}^{m4} + z_{pq}^{m5} + z_{pq}^{m6} + z_{pq}^{m7} + z_{pq}^{m8} + z_{pq}^{m9} + z_{pq}^{m10} + z_{pq}^{m11}$$

The first sequence impedance

$$z_{pq}^1 = z_{pq}^s + az_{pq}^{m1} + a^2 z_{pq}^{m2} + az_{pq}^{m3} - a^2 z_{pq}^{m4} - az_{pq}^{m5} - z_{pq}^{m6} - az_{pq}^{m7} - a^2 z_{pq}^{m8} - az_{pq}^{m9} + a^2 z_{pq}^{m10} + az_{pq}^{m11}$$

and so on.

Proposition: The transformation matrix A_c which diagonalizes the coefficient matrix of 12-phase rotating element network, is a linear power invariant transformation matrix with complex elements similar to the symmetrical components for 3-phase system.

4.2 12-PHASE STATIONARY ELEMENTS

Power system stationary elements possess rotational as well as reflection symmetries (typical example is that of 12-transposed transmission line). These symmetries can be represented by permutation matrices $D(R)$ (eqns. 2.5 and 2.7) as seen last chapter. In the previous section we have seen that impedance matrix for 12-phase network with rotational symmetry is cyclic (eqn.4.3). Now, for networks possessing reflection

symmetries in addition to rotational ones, applying (3.1)

for $R = \delta'_a, \delta'_b, \delta'_c, \delta'_d, \delta'_e, \delta'_f, \delta'_g, \delta'_h, \delta'_i, \delta'_j, \delta'_k, \delta'_l$ and making term by term comparison in

$$[Z_{pq}]^{\text{phase}} = D^{-1}(R)[Z_{pq}]_{\text{phase}} D(R)$$

$$\text{for } R = \delta'_a, \delta'_b, \dots, \delta'_l$$

We get that $[Z_{pq}]$ is of the form:

$$[Z_{pq}]_{\text{phase}} =$$

$$\begin{bmatrix} z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s & z_{pq}^m \\ z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^m & z_{pq}^s \end{bmatrix}$$

(4.10)

The twenty four symmetry operations form the group C_{12v} of order twenty four but there are only nine classes viz. $[D(E)]$; $[D(C_{12}^1), D(C_{12}^{11})]$; $[D(C_{12}^2), D(C_{12}^{10})]$; $[D(C_{12}^3), D(C_{12}^9)]$; $[D(C_{12}^4), D(C_{12}^8)]$; $[D(C_{12}^5), D(C_{12}^7)]$; $[D(C_{12}^6)]$; $[D(\delta'_a), D(\delta'_b), D(\delta'_c), D(\delta'_d), D(\delta'_e), D(\delta'_f)]$; $[D(\delta'_g), D(\delta'_h), D(\delta'_i), D(\delta'_j), D(\delta'_k), D(\delta'_l)]$. Therefore the number of irreducible representation is also nine. Let l_1, l_2, \dots, l_9 be the dimensions of these irreducible representations. Then, from eqn.(3.7), we have

$$\sum_{i=1}^9 l_i^2 = l_1^2 + l_2^2 + \dots + l_9^2 = h = 24$$

The solution of this equation is $l_1 = l_2 = l_3 = l_4 = 1$ and $l_5 = l_6 = l_7 = l_8 = l_9 = 2$. From this we conclude that there are four irreducible representations viz. $D^1(R), D^2(R), D^3(R), D^4(R)$ of dimension 1 each and five irreducible representations viz. $D^5(R), D^6(R), D^7(R), D^8(R),$ and $D^9(R)$ of dimension 2 each. From eqn.(3.8),

$$\sum_R X_i^2(R) = h = 24$$

So, the character of each of twenty four of first four irreducible representations whose dimension is 1 is of unity modulus, but of the last five representations whose dimension is 2, is 2, -2 or 0. Now, we write character table using orthogonality theorem (Appendix 2) and its consequences.

C_{12V}	\mathbb{R}	C_{12}^1	C_{12}^2	C_{12}^3	C_{12}^4	C_{12}^5	C_{12}^6	C_{12}^7	C_{12}^8	C_{12}^9	C_{12}^{10}	C_{12}^{11}	δ'_a	δ'_b	δ'_c	δ'_d	δ'_e	δ'_f	δ'_g	δ'_h	δ'_i	δ'_j	δ'_k	δ'_l
$X^1(R)$	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
$X^2(R)$	1	1	1	1	1	1	1	1	1	1	1	1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
$X^3(R)$	1	-1	1	-1	1	-1	1	-1	1	-1	1	-1	1	1	1	1	1	1	1	-1	-1	-1	-1	-1
$X^4(R)$	1	-1	1	-1	1	-1	1	-1	1	-1	1	-1	-1	-1	-1	-1	-1	-1	1	1	1	1	1	1
$X^5(R)$	2	1	-1	-2	-1	1	2	1	-1	-2	-1	1	0	0	0	0	0	0	0	0	0	0	0	0
$X^6(R)$	2	-1	-1	2	-1	-1	2	-1	-1	2	-1	-1	0	0	0	0	0	0	0	0	0	0	0	0
$X^7(R)$	2	0	-2	0	2	0	-2	0	2	0	-2	0	0	0	0	0	0	0	0	0	0	0	0	0
$X^8(R)$	2	1	1	-2	-1	-1	-2	-1	-1	2	1	1	0	0	0	0	0	0	0	0	0	0	0	0
$X^9(R)$	2	-1	1	2	-1	1	-2	1	-1	-2	1	-1	0	0	0	0	0	0	0	0	0	0	0	0
Red. Rep $X(R)$	12	0	0	0	0	0	0	0	0	0	0	0	2	2	2	2	2	2	2	0	0	0	0	0

CHARACTER TABLE

(4.11)

It is evident that irreducible representations whose dimension is 1, are the same as their characters. Irreducible representations, whose dimension is 2 are found by using orthogonality theorem and its consequences (Appendix 2) and Cayley's table. To find the irreducible representations, first we find irreducible representation for rotational symmetries and by using Cayley's table irreducible representations for reflection symmetries are found. The irreducible representations in the final form are given by equation (4.12).

The number of times each of the irreducible representation $D^i(R)$ appears at the diagonal of $\bar{D}(R)$ is determined by eqn.(3.10), and thus we obtain,

$$a_1 = 1, a_2 = 0, a_3 = 1, a_4 = 0, a_5 = a_6 = a_7 = a_8 = a_9 = 1$$

Let the transformation matrix be A_r , then

$$\bar{D}(R) = A_r^{*T} D(R) A_r = \begin{bmatrix} D^1(R) & & & & & & & & \\ & D^3(R) & & & & & & & \\ & & D^5(R) & & & & & & \\ & & & D^6(R) & & & & & \\ & & & & D^7(R) & & & & \\ & & & & & D^8(R) & & & \\ 0 & & & & & & D^9(R) & & \end{bmatrix} \quad (4.13)$$

After this we determine matrix G_i^j following the procedure outlined earlier and thus obtain $G_1^1, G_2^1, G_3^1, G_4^1, G_5^1, G_5^2, G_6^1, G_6^2, G_7^1, G_7^2, G_8^1, G_8^2, G_9^1, \text{ and } G_9^2$.

The basis vector α_{mnp} is also found in the similar manner and comes out to be the following:

$$\alpha_{111} = \frac{1}{\sqrt{12}} [1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1]^T$$

$$\alpha_{311} = \frac{1}{\sqrt{12}} [1 \ -1 \ 1 \ -1 \ 1 \ -1 \ 1 \ -1 \ 1 \ -1 \ 1 \ -1]^T$$

$$\alpha_{511} = \frac{1}{\sqrt{12}} \left[\sqrt{2} \ \frac{1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ -\sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{1}{\sqrt{2}} \ \sqrt{2} \ \frac{1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ -\sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{1}{\sqrt{2}} \right]^T$$

$$\alpha_{521} = \frac{1}{\sqrt{12}} [0 \ \frac{\sqrt{3}}{2} \ \frac{\sqrt{3}}{2} \ 0 \ -\frac{\sqrt{3}}{2} \ -\frac{\sqrt{3}}{2} \ 0 \ \frac{\sqrt{3}}{2} \ \frac{\sqrt{3}}{2} \ 0 \ -\frac{\sqrt{3}}{2} \ -\frac{\sqrt{3}}{2}]^T$$

$$\alpha_{611} = \frac{1}{\sqrt{12}} \left[\sqrt{2} \ -\frac{1}{\sqrt{2}} \ -\frac{1}{\sqrt{2}} \ \sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ \sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ \sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \right]^T$$

$$\alpha_{621} = \frac{1}{\sqrt{12}} [0 \ \frac{\sqrt{3}}{2} \ -\frac{\sqrt{3}}{2} \ 0 \ \frac{\sqrt{3}}{2} \ -\frac{\sqrt{3}}{2} \ 0 \ \frac{\sqrt{3}}{2} \ -\frac{\sqrt{3}}{2} \ 0 \ \frac{\sqrt{3}}{2} \ -\frac{\sqrt{3}}{2}]^T$$

$$\alpha_{711} = \frac{1}{\sqrt{12}} [\sqrt{2} \ 0 \ -\sqrt{2} \ 0 \ \sqrt{2} \ 0 \ -\sqrt{2} \ 0 \ \sqrt{2} \ 0 \ -\sqrt{2} \ 0]^T$$

$$\alpha_{721} = \frac{1}{\sqrt{12}} [0 \ \sqrt{2} \ 0 \ -\sqrt{2} \ 0 \ \sqrt{2} \ 0 \ -\sqrt{2} \ 0 \ \sqrt{2} \ 0 \ -\sqrt{2}]^T$$

$$\alpha_{811} = \frac{1}{\sqrt{12}} \left[\sqrt{2} \ \frac{1}{\sqrt{2}} \ \frac{\sqrt{1}}{2} \ -\sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ -\sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ \sqrt{2} \ \frac{1}{\sqrt{2}} \ \frac{1}{\sqrt{2}} \right]^T$$

$$\alpha_{821} = \frac{1}{\sqrt{12}} [0 \ \frac{1}{2}\frac{\sqrt{3}}{2} \ \frac{3}{2}\frac{\sqrt{3}}{2} \ \frac{\sqrt{3}}{2} \ \frac{-1}{2}\frac{\sqrt{3}}{2} \ \frac{1}{2}\frac{\sqrt{3}}{2} \ 0 \ \frac{1}{2}\frac{\sqrt{3}}{2} \ \frac{-3}{2}\frac{\sqrt{3}}{2} \ \frac{-\sqrt{3}}{2} \ \frac{1}{2}\frac{\sqrt{3}}{2} \ \frac{-1}{2}\frac{\sqrt{3}}{2}]$$

$$\alpha_{911} = \frac{1}{\sqrt{12}} \left[\sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{1}{\sqrt{2}} \ \sqrt{2} \ \frac{-1}{\sqrt{2}} \ \frac{1}{\sqrt{2}} \ -\sqrt{2} \ \frac{1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \ -\sqrt{2} \ \frac{1}{\sqrt{2}} \ \frac{-1}{\sqrt{2}} \right]^T$$

and

$$\alpha_{921} = \frac{1}{\sqrt{12}} \left[0 \quad \frac{1}{2}\sqrt{3} \quad -\frac{3}{2}\sqrt{3} \quad \frac{\sqrt{3}}{2} \quad \frac{1}{2}\sqrt{3} \quad \frac{1}{2}\sqrt{3} \quad 0 \quad -\frac{1}{2}\sqrt{3} \quad \frac{3}{2}\sqrt{3} \quad -\frac{\sqrt{3}}{2} \quad -\frac{1}{2}\sqrt{3} \quad -\frac{1}{2}\sqrt{3} \right]^T$$

Therefore, transformation matrix $A_r = \text{matrix } \alpha =$

$$\begin{bmatrix} \alpha_{111} & \alpha_{311} & \alpha_{511} & \alpha_{521} & \alpha_{611} & \alpha_{621} & \alpha_{711} & \alpha_{721} & \alpha_{811} & \alpha_{821} & \alpha_{911} & \alpha_{921} \end{bmatrix}$$

$$\begin{matrix} D^1(R) & D^3(R) & D^5(R) & D^6(R) & D^7(R) & D^8(R) & D^9(R) \end{matrix}$$

$$= \frac{1}{\sqrt{12}} \begin{bmatrix} 1 & 1 & \sqrt{2} & 0 & \sqrt{2} & 0 & \sqrt{2} & 0 & \sqrt{2} & 0 & \sqrt{2} & 0 \\ 1 & -1 & \frac{1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & 0 & \sqrt{2} & \frac{1}{\sqrt{2}} & \frac{1}{2}\sqrt{3} & \frac{-1}{\sqrt{2}} & \frac{1}{2}\sqrt{3} \\ 1 & 1 & \frac{-1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & -\sqrt{2} & 0 & \frac{1}{\sqrt{2}} & \frac{3}{2}\sqrt{3} & \frac{1}{\sqrt{2}} & \frac{-3}{2}\sqrt{3} \\ 1 & -1 & -\sqrt{2} & 0 & \sqrt{2} & 0 & 0 & -\sqrt{2} & -\sqrt{2} & \frac{\sqrt{3}}{2} & \sqrt{2} & \frac{\sqrt{3}}{2} \\ 1 & 1 & \frac{-1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & \sqrt{2} & 0 & \frac{-1}{\sqrt{2}} & \frac{-1}{2}\sqrt{3} & \frac{-1}{\sqrt{2}} & \frac{1}{2}\sqrt{3} \\ 1 & -1 & \frac{1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{-3}{2} & 0 & -\sqrt{2} & \frac{-1}{\sqrt{2}} & \frac{1}{2}\sqrt{3} & \frac{1}{\sqrt{2}} & \frac{1}{2}\sqrt{3} \\ 1 & 1 & \sqrt{2} & 0 & \sqrt{2} & 0 & -\sqrt{2} & 0 & -\sqrt{2} & 0 & -\sqrt{2} & 0 \\ 1 & -1 & \frac{1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & 0 & \sqrt{2} & \frac{-1}{\sqrt{2}} & \frac{-1}{2}\sqrt{3} & \frac{1}{\sqrt{2}} & \frac{-1}{2}\sqrt{3} \\ 1 & 1 & \frac{-1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & \sqrt{2} & 0 & \frac{-1}{\sqrt{2}} & \frac{-3}{2}\sqrt{3} & \frac{-1}{\sqrt{2}} & \frac{3}{2}\sqrt{3} \\ 1 & -1 & -\sqrt{2} & 0 & \sqrt{2} & 0 & 0 & -\sqrt{2} & \sqrt{2} & \frac{-\sqrt{3}}{2} & -\sqrt{2} & \frac{-\sqrt{3}}{2} \\ 1 & 1 & \frac{-1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{\sqrt{3}}{2} & -\sqrt{2} & 0 & \frac{+1}{\sqrt{2}} & \frac{1}{2}\sqrt{3} & \frac{1}{\sqrt{2}} & \frac{-1}{2}\sqrt{3} \\ 1 & -1 & \frac{1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & \frac{-1}{\sqrt{2}} & \frac{-\sqrt{3}}{2} & 0 & \sqrt{2} & \frac{+1}{\sqrt{2}} & \frac{-1}{2}\sqrt{3} & \frac{-1}{\sqrt{2}} & \frac{-1}{2}\sqrt{3} \end{bmatrix}$$

It can be verified that $A_r^T A_r = I = A_r^{-1} A_r$. Therefore, the transformation matrix A_r is orthogonal. From equation (3.17),

$$[Z_{pq}]_{\text{comp}} = A_r^{*T} [Z_{pq}]_{\text{phase}} A_r$$

Substituting for $[Z_{pq}]_{\text{phase}}$ from equation (4.10) and A_r from (4.14) and then performing the matrix multiplications, we get

$$[Z_{pq}]_{\text{comp}}^{0,1,2,3,4,5,6,7,8,9,10,11} =$$

$$= \begin{bmatrix} z_{pq}^s + 11z_{pq}^m & & & & & & & & & & & \\ & z_{pq}^s - z_{pq}^m & & & & & & & & & & \\ & & z_{pq}^s - z_{pq}^m & & & & & & & & & \\ & & & z_{pq}^s - z_{pq}^m & & & & & & & & \\ & & & & z_{pq}^s - z_{pq}^m & & & & & & & \\ & & & & & z_{pq}^s - z_{pq}^m & & & & & & \\ & & & & & & z_{pq}^s - z_{pq}^m & & & & & \\ & & & & & & & z_{pq}^s - z_{pq}^m & & & & \\ & & & & & & & & z_{pq}^s - z_{pq}^m & & & \\ & & & & & & & & & z_{pq}^s - z_{pq}^m & & \\ & & & & & & & & & & z_{pq}^s - z_{pq}^m & \\ & & & & & & & & & & & z_{pq}^s - z_{pq}^m \\ & & & & & & & & & & & & 0 \end{bmatrix} \quad (4.15)$$

From this, it is clear that the transformation matrix A_r diagonalizes the coefficient matrix $[Z_{pq}]$ of 12-phase stationary elements.

It is to be noted here that the matrix A_c derived earlier can also diagonalize $[Z_{pq}]$ since the stationary elements also possess rotational symmetries in addition to reflection ones. The diagonal elements of $[Z_{pq}]_{comp}$ are the sequence impedances in this case. More specifically, the zero sequence impedance

$$z_{pq}^0 = z_{pq}^s + 11 z_{pq}^m$$

First sequence impedance $z_{pq}^1 = z_{pq}^s - z_{pq}^m$

The second to eleventh sequence impedances are same as z_{pq}^1 i.e. first sequence impedance.

Complex Power

The complex power in the 12-phase stationary element p-q

$$\begin{aligned} S_{pq} &= P_{pq} - jQ_{pq} = [\bar{v}_{pq}^{abcdefghijkl}]^{*T} [\bar{i}_{pq}^{abcdefghijkl}] \\ &= [A_r \cdot \bar{v}_{pq}^{0,1,2,3,4,5,6,7,8,9,10,11}]^{*T} [A_r \bar{i}_{pq}^{0,1,2,3,4,5,6,7,8,9,10,11}] \\ &= [\bar{v}_{pq}^{0,1,2,3,4,5,6,7,8,9,10,11}]^{*T} A_r^{*T} A_r x \\ &\quad [\bar{i}_{pq}^{0,1,2,3,4,5,6,7,8,9,10,11}] \\ &= [\bar{v}_{pq}^{0,1,2,3,4,5,6,7,8,9,10,11}]^{*T} x \\ &\quad [i_{pq}^{0,1,2,3,4,5,6,7,8,9,10,11}] \end{aligned} \quad (4.16)$$

because $A_r^* = A_r$ and $A_r^{*T} A_r = A_r^T A_r = I$ i.e. $A_r^{-1} = A_r^T$.

Thus we conclude,

Proposition: The orthogonal matrix A_r which transforms the field of phasors of a 12-phase system to the field of components is a linear power invariant real transformation matrix similar to Clarke's component transformation matrix of 3-phase systems.

Remark: Similar expression for complex power is also obtained using complex transformation matrix A_c .

CHAPTER 5

CONCLUSION

The inherent symmetries associated with the power system networks enable us to simplify the analysis of multiphase power system networks by application of group theoretic techniques. An attempt has been made in this thesis to make use of this fact in the steady state analysis of multiphase power system networks.

The methods developed earlier, for 4-phase and 6-phase power systems have been used here for analysis of 8-phase and 12-phase systems. Based on the fact that symmetries of n -phase power system network with rotational elements constitute a cyclic group G_n and that of networks with stationary elements constitute a group G_{nv} , similarity transformations with complex elements as well as real elements for 8 phase and 12 phase power system networks have been developed using group theoretic techniques. The main advantage of using group theoretic techniques is that they are applicable in a unified manner to multiphase system which seem to have a bright future. The similarity transformations developed here are linear and power invariant.

Amongst the new directions in which these techniques may be applied is one of transient analysis of multiphase systems by using the symmetries of network under transient conditions. Another direction in which the techniques

used in this thesis may have a possible application is in the analysis of network with nonlinear elements such as saturable core reactors. These elements although nonlinear, do exhibit symmetries analogous to those of the linear elements. With the help of approximate matrix representation of these symmetries, the analysis of networks containing nonlinear elements is likely to be considerably simplified.

REFERENCES

1. Singh, L.P., 'Group theoretic considerations in the analysis of power system network' Ph.D. Thesis, submitted to Elect. Engg.Dept., I.I.T.Kanpur.
2. Venkata, S.S., Bhatt, N.B. and Guyker, W.C, '6-phase (multi-phase) power transmission system: concept and reliability aspects', presented at the IEEE Summer Power Meeting, Portland, Ore., July 18-23.
3. Barthold, .D. and Barnes, H.C., 'High phase order transmission', CIGRE study committee, No.31 Report, London.
- 4.S Singh, L.P. and Sinha, V.P., 'Transient analysis of power system network using group theoretic approach', accepted by Jr.of Inst. of Engrs., India.
5. Singh, L.P. and Sinha, V.P., 'Analysis of multiphase power system networks', accepted by IFAC, Symposium on Computer applications in large scale power systems to be held at New Delhi, August 16-17, 1979.
6. Fortescue, C.L., 'Method of symmetrical components applied to the solution of polyphase networks', Trans. AIEE, Vol.XXXVII, Part II, pp.1027-1140, 1918.
7. Clarke, Edith, 'Circuit Analysis of A.C.Power Systems, Symmetrical and Related Components', Vol.John Wiley and Sons, New York, 1943.
8. Jurtis, J.W., 'Representation Theory of Finite Groups and Associative Algebra', John Wiley and Sons, N.Y., 1962.
9. Hamermesh, M., 'Group Theory and Its Applications and Physical Problems', Addison-Wesley, Pub.Co.Inc., Mass.1962.
10. Howitt, N., 'Group theory and the electric circuit', Phys.Rev., Vol.37, pp.1583-1595, June 15, 1931.
11. Mirsky, L., 'An Introduction to the Linear Algebra', Clayendon Press, Oxford Univ, London, 1961.
12. Kerns, D.M., 'Analysis of symmetrical waveguide junctions', Journal of Research of the National Bureau of Standards, Vol.46, pp. 267-282, April 1951.

13. Lomont, J.S., 'Applications of finite groups', Academic Press, New York, 1959.
14. Higman, B., 'Applied Group Theoretic and Matrix Methods', Dover Publications Inc., New York, 1955.
15. Tinkham, M., 'Group Theory and Quantum Mechanics', Mc-Graw Hill Book Co. Inc., New York, 1964.
16. Rubin, H., 'Symmetric linear time-variable networks and the theory of finite groups', Technical report no.117, Dept.of Electrical Engg., Columbia Univ.

APPENDIX 1

We give here a brief review of the mathematical theory of groups used in this thesis. We start first with the definition and properties of the finite group. For details, reader are required to refer to the references [1,16].

1. GROUP: Suppose we are given a set G . Let $'.'$ (commonly known as multiplication) be the binary operation defined on the set G . Then set G is said to be a group if it satisfies the following postulates, called group axioms:

(i) Closure: Given any two elements a and b of the set G , $a.b$ the result of the binary operation on a and b is also in G .

(ii) Associativity: For elements a, b and c of set G , we have the following relation,

$$a.(b.c) = (a.b).c$$

(iii) Existence of Identity: Among the elements of the set G , there exists an element e called identity element such that

$$a.e. = e.a = a$$

and (iv) Existence of Inverse: Corresponding to every element a of the set G , there exists an element a^{-1} , called the inverse of the element a of the set G such that

$$a.a^{-1} = a^{-1}a = e$$

If, in addition to the above four group axioms, the following condition is also satisfied, then the group is known as commutative or abelian group.

(v) Commutativity: For any element a and b in the group G , we have

$$a.b = b.a$$

If the number of elements is finite in the group, then the group is said to be finite and then the number of distinct elements in the finite group is called the order of the group.

Group Multiplication Table:

For a finite group G with binary operation of multiplication, the multiplications of group elements and their products can most conveniently be presented in a table known as a group multiplication table. The group elements are arranged along the column and the row of the table. The entry in the i - j th position of the table is the group element $p_i.p_j$ which results from multiplication of p_i , an element in the i th row and p_j , an element in the j th row. For a completely and uniquely defined group, its elements which may have physical interpretation, can be represented by abstract quantities viz. a, b, c, \dots etc.

Cyclic Group:

A cyclic group is one in which all elements are generated by a single element, known as a generating element or simply a generator. For example, the set G with elements as 4th root of unity $(1, a, a^2, a^3)$ where $a = e^{j2\pi/4}$ constitute a cyclic group under multiplication and element a is the generator element.

Classes:

Two elements a and b of a group G are conjugate if there exists another element X in G such that

$$b = X^{-1}aX$$

Conjugate elements have following properties:

- (i) Every element is conjugate with itself.
- (ii) If the element a is conjugate to b , then the element b will also be conjugate to a .

and

- (iii) If a is conjugate to both b and c , then b and c are conjugate to one another.

A complete set of elements of a group G which are conjugate to one another is called a class of the group.

Note: The orders of all classes in a group, are integral factors of the order of the group.

APPENDIX 2

ORTHOGONALITY THEOREM

Several important properties of group representations and their characters are derived from basic theorem concerning elements of matrices which constitute irreducible representations of the group. This theorem is known as orthogonality theorem and is stated as follows:

$$\sum_R D^i(R)_{mn} D^j(R)_{m'n'}^* = \frac{h^2}{\sqrt{l_i l_j}} \delta_{ij} \delta_{mm'} \delta_{nn'} \quad (\text{A-2.1})$$

where h is the order of the group and l_i is the dimension of the i th irreducible representation which is the order of each of the matrices constituting i th representation, $D^i(R)_{mn}$ is the element in the m th row and n th column of $D^i(R)$, the matrix corresponding to symmetry operation R in the i th irreducible representation. Eqn.(A2.1) of the orthogonality theorem can be split up into three simpler relations as shown below,

$$\sum D^i(R)_{mn} D^j(R)_{mn}^* = 0 \quad \text{for } i \neq j \quad (\text{A-2.2})$$

$$\sum D^i(R)_{mn} D^i(R)_{m'n'}^* = 0 \quad \text{if } m \neq m' \text{ and } n \neq n' \quad (\text{A-2.3})$$

$$\sum D^i(R)_{mn} D^i(R)_{mn}^* = h^2/l_i \quad (\text{A-2.4})$$